

GEOTECHNOLOGY



GEOTECHNICAL DATA REPORT SR-222 FROM NEAR SR-468 TO NEAR CAMPGROUND RD HAYWOOD COUNTY, TENNESSEE

**TDOT PROJECT No. R4S222-S1-002
TDOT PIN No. 132709.00
TDOT GES No. 3805723**

Prepared for:

**FISHER ARNOLD, INC.
MEMPHIS, TENNESSEE**

Prepared by:

**GEOTECHNOLOGY, LLC
MEMPHIS, TENNESSEE**

Date:

MARCH 9, 2023

Geotechnology Project No.:

J042140.01

**SAFETY
QUALITY
INTEGRITY
PARTNERSHIP
OPPORTUNITY
RESPONSIVENESS**



March 9, 2023

Mr. John Pankey, P.E.
Fisher Arnold, Inc.
9180 Crestwyn Hills Drive
Memphis, Tennessee 38125

Re: Geotechnical Data Report
SR-222 From Near SR-468 To Near Campground Rd
Haywood County, Tennessee
Geotechnology Project No. J042140.01
TDOT Project No. R4S222-S1-002
TDOT Pin No. 132709.00
TDOT GES No. 3805723

Dear Mr. Pankey:

Presented in this report are the results of the geotechnical exploration performed by Geotechnology, LLC for the referenced project. The report includes our understanding of the project, observed site conditions, and support data as listed in the Table of Contents.

We appreciate the opportunity to provide geotechnical services for this project. If you have any questions regarding this report, or if we can be of any additional service to you, please do not hesitate to contact us.

Respectfully submitted,

GEOTECHNOLOGY, LLC

Amber Meadows
Project Engineer

Ashraf S. Elsayed, Ph.D., P.E.
Chief Engineer – South Region

ABM/ASE:abm

Copies submitted: Client (email)



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**Geotechnical Data Report
SR-222 From Near SR-468 To Near Campground Rd
Haywood County, Tennessee**

March 9, 2023 | Geotechnology Project No. J042140.01

1.0 SCOPE OF SERVICES

Presented in this report are the results of the geotechnical exploration for the proposed improvements and widening of SR-222. The project location is shown on Figure 1 included in Appendix B.

A total of 48 borings were performed in the vicinity of the site as shown on Figures 2 through 12 included in Appendix B. The boring logs, along with field and laboratory test results, are enclosed. Unless noted otherwise, all dimensions, measurements, depths, and locations in this report should be considered approximate. Important information prepared by the Geotechnical Business Council (GBC) of the Geoprofessional Business Association for studies of this type is presented in Appendix A for your review.

2.0 GENERAL INFORMATION

Planned Modifications

The project extends along SR-222 from approximately two miles north of its intersection with I-40 to ¼-mile north of its intersection with Campground Road.

Geology

The site is located in Haywood County in southwestern Tennessee on the Gulf Coastal Plain. The Coastal Plain in the project area is characterized by flat to hilly topography and many rivers and creeks. Approximately 200 feet of relief occur across the county.

Geologically, the site is near the north-central part of the Mississippi Embayment, a trough-like depression plunging southward along an axis approximating the present course of the Mississippi River. Sediment depth in the project area is approximately 2,900 feet. The unconsolidated sediments consist of clay, silt (aeolian, alluvial and marine), sand, gravel and lignite. Except for some local beds of ferruginous and calcareous sandstone, there is no well-consolidated rock above the Paleozoic Formation, which forms the rock below the sediments.

The uppermost formation over most of Haywood County is Pleistocene Epoch Loess, which consists of clayey silts and silty clays. Loess is predominantly silt, but with varying amounts of clay, and is generally buff-colored and uniform in texture. The thickness of the loess is usually about 20 to 30 feet, but typically is greater than 60 feet along the Mississippi River. The loess cap thins to the east, commonly terminating at the Mississippi Embayment boundary.



The next formation in succession is a discontinuous series of alluvial deposits referred to as the Terrace Deposits. The terrace deposits are tertiary period in age, thin gradually eastward, and are absent in many places as a result of erosion or non-deposition. The alluvial deposits are composed mostly of coarse-grained quartz sand, fine-grained iron-stained quartz and chert gravel. Lenses of yellowish-brown clay are frequently present locally in the lower part of the deposits. These materials are typically red or brown, dense and well graded, and the thickness ranges from 0 to 200 feet. They generally occur 35 to 50 feet below the ground surface.

Underlying the terrace deposits is the Tertiary Period Claiborne/Wilcox Formation, which is characterized as sand layers interbedded with gray to white clay, silty clay, lignitic clay, and lignite. The Claiborne/Wilcox Formation is typically more than 400 feet thick.

Sediments deposited by streams along the channels and on the flood plains during flood periods are referred to as Alluvium. These materials are from the Holocene Period, and are composed of clay, silt, sand, and gravel. The alluvium in the Memphis area is generally confined to strips along the Mississippi River and its tributaries, and it is frequently subjected to flooding and reworking. Lignite, peat, and carbonaceous materials are distributed irregularly throughout the upper level. Alluvial sands are usually white or gray, loose to medium dense, and poorly graded. The loose and poorly graded alluvial sands can be susceptible to liquefaction during seismic events.

3.0 GEOTECHNICAL EXPLORATION

The geotechnical exploration consisted of 58 borings, designated as Borings BR-1, -2, W-1A, -1B, -2, -3A, -3B, -4 through -21, E-1 through -16, CON-1 through -7, and SP-1 through -10. The borings were drilled along the edge of the pavement and in the shoulders of the existing roadway in the project area between December 13, 2022 and January 26, 2023. Borings CON-1 through -7 were drilled along the edge of the pavement of Stanton-Somerville Road. Borings SP-1 through -10 were drilled for the signal poles at the planned BO entrances and improved Stanton-Somerville intersection. Approximate locations of the borings are shown on Figures 2 through 12 in Appendix B and summarized in Table 1. The coordinates and depth of each boring location are also summarized in Appendix B.

Table 1. Boring Locations.

Number of Borings	Boring Location
24	SR 222 Westbound Shoulder
15	SR 222 Eastbound Shoulder
2	Box Culvert
2	Blue Oval 1 Intersection
2	Blue Oval 2 Intersection
3	Stanton-Somerville Southbound Shoulder
4	Signal Poles - SR 222 Westbound Shoulder
6	Signal Poles - SR 222 Eastbound Shoulder



The borings were drilled with track- and ATV-mounted rotary drill rigs using hollow stem auger and rotary wash drilling methods to a maximum depth of 80 feet. Sampling procedures included Standard Penetration Test (SPT) and thin-walled (Shelby) tube methods. SPT's were conducted at 2.5- and 5-foot depth intervals using an automatic hammer to obtain the standard penetration resistance, or N-values¹, of the sampled material. Pavement cores were also obtained at selected locations along SR 222. Samples collected by Geotechnology were visually examined by a geologist and transported to our laboratory for further evaluation and testing. The samples were examined in the laboratory by a geotechnical professional who prepared descriptive logs of the materials encountered. Logs of the borings are presented in Appendix C. An explanation of the terms and symbols used on the boring logs is also provided in Appendix C. Listed in Table 2 are in situ tests and measurements made as part of the fieldwork and recorded on the boring logs. Descriptions and photographs of the pavement cores are provided in Section 5.0 and Appendix E, respectively.

Table 2. Field Tests and Measurements.

Item	Test Method
Soil Classification	ASTM D 2488/ D 3282
Standard Penetration Test (SPT)	ASTM D 1586/ AASHTO T206
Thin-Walled (Shelby) Tube Sampling	ASTM D 1587/ AASHTO T207
Phreatic Surface Level Measurement in Boring	ASTM D 4750

The boring logs and related information depict subsurface conditions only at the specific locations and times where sampling was conducted. The passage of time could result in changes in conditions, interpreted to exist, at or between the locations where sampling was conducted.

4.0 LABORATORY REVIEW AND TESTING

Laboratory testing was performed on soil samples to assess engineering and index properties. Moisture contents, Atterberg limits, percent fines, pH, resistivity, and UU test results are presented on the boring logs in Appendix C. Laboratory test results for Atterberg, grain size (sieve) analysis, resistivity, moisture-density (proctor), CBR, and unconsolidated-undrained triaxial compression (UU), are presented in Appendix D. Laboratory tests and corresponding test method standards are listed in Table 3.

¹ The standard penetration resistance, or N-value, is defined as the number of blows required to drive the split-spoon sampler 12 inches with a 140-pound hammer falling 30 inches. Since the split spoon sampler is driven 18 inches or until refusal, the blows for the first 6 inches are for seating the sampler, and the number of blows for the final 12 inches is the N-value. Additionally, "refusal" of the split-spoon sampler occurs when the sampler is driven less than 6 inches with 50 blows of the hammer.

**Table 3. Summary of Laboratory Tests and Methods.**

Laboratory Test	ASTM	AASHTO
Moisture Content	D 2216	T 265
Atterberg Limits	D 4318	T 98
Grain Size Analysis by Sieving	D 6913	T 88
Unconsolidated-Undrained Triaxial Compression (UU)	D 2850	T 296
Soil Electrical Resistivity	G 57	T 288
Soil pH	D 4972	T 289
Moisture-Density (Standard Effort)	D 698	T 99
California Bearing Ratio (CBR)	D 1883	T 193

The boring logs were prepared from field logs, visual classification of the soil samples, and laboratory test results. Terms and symbols used on the boring logs are presented on the Boring Log: Terms and Symbols in Appendix C. Stratification lines on the boring logs indicate approximate changes in strata. The transition between materials could be gradual or could occur between recovered samples. The stratification given on the boring logs, or described herein, is for use by Geotechnology in its analyses and should not be used as the basis of design or construction cost estimates without realizing that there can be variation from that shown or described.

5.0 EXPLORATION RESULTS

Pavement Information

Core samples were collected from the existing SR-222 pavement near the locations of Borings E-1, E-7, W-5, W-10, and W-21. Borings E-12, E-14, W-16, W-19, and W-20 were drilled in the existing pavement along SR-222 and CON-5 through -7 were drilled in the existing pavement along Stanton-Somerville Road. The approximate thickness of asphalt measured from the pavement cores and in the borings are shown in Table 4. Photographs of the pavement cores are provided in Appendix E.

**Table 4. Approximate Asphaltic Material Thicknesses.**

Boring	Location	SR-222 Station (feet)	Total Asphalt Thickness (inches)
E-1 ^a	SR-222	3042+05	4½
E-7 ^a		3095+69	4¼
E-12		3117+50	10
E-14		3131+30	10
W-5 ^a		3072+59	4¾
W-10 ^a		3093+08	5
W-16		3118+83	10
W-19		3136+45	6
W-20		3139+48	10
W-21 ^a		3143+30	17
CON-5	Stanton-Somerville Road	3118+52	10
CON-6		3118+28	6
CON-7		3118+09	10

^a Pavement core

General Stratigraphy

The stratigraphy encountered in the borings generally consisted of intermixed layers of predominantly fine-grained soils classified as clayey silt (ML), lean clay (CL), fat clay (CH), and sandy clay (CL/CH) and predominantly coarse-grained soils classified as clayey sand (SC), sand with clay (SP-SC), and silty sand (SM). In some areas the stratigraphy encountered in the borings consisted of predominantly fine-grained soils and fine-grained soils underlain by predominantly coarse-grained soils. Detailed descriptions of the stratigraphy encountered are presented on the boring logs Appendix C.

Groundwater

Groundwater was encountered during drilling at approximate depths of 6, 10, and 23 feet (El 313 to El 285) in Borings SP-8, SP-5, and BR-1, respectively. Groundwater levels vary over time due to seasonal variation in precipitation, recharge, or other factors not evident at the time of exploration.

6.0 LIMITATIONS

This report has been prepared on behalf of, and for the exclusive use of, the client for specific application to the named project as described herein. If this report is provided to other parties, it should be provided in its entirety with all supplementary information. In addition, the client should make it clear the information is provided for factual data only, and not as a warranty of subsurface conditions presented in this report.

Geotechnology has attempted to conduct the services reported herein in a manner consistent with the level of care and skill ordinarily exercised by members of the profession currently



practicing in the same locality and under similar conditions. The report is not a bidding document and should not be used for that purpose.

Our scope for this phase of the project did not include any environmental assessment or investigation for the presence or absence of wetlands or hazardous or toxic materials in the soil, surface water, groundwater, or air, on or below or around this site. Any statements in this report or on the boring logs regarding odors noted or unusual or suspicious items or conditions observed are strictly for the information of our client. Our scope did not include an assessment of the effects of flooding and erosion of creeks or rivers adjacent to or on the project site.

Our scope did not include: any services to investigate or detect the presence of mold or any other biological contaminants (such as spores, fungus, bacteria, viruses, and the by-products of such organisms) on and around the site; or any services, designed or intended, to prevent or lower the risk of the occurrence of an infestation of mold or other biological contaminants.

The information contained in this report is based on the data obtained from the geotechnical exploration. The field exploration methods used indicate subsurface conditions only at the specific locations where samples were obtained, only at the time they were obtained, and only to the depths penetrated. Consequently, subsurface conditions could vary gradually, abruptly, and/or nonlinearly between sample locations and/or intervals.

The information presented in this report should not be used without Geotechnology's review and assessment if the nature, design, or location of the facilities is changed, if there is a lapse in time between the submittal of this report and the start of work at the site, or if there is a substantial interruption or delay during work at the site. If changes are contemplated or delays occur, Geotechnology must be allowed to review them to assess their impact on the findings given in this report. Geotechnology will not be responsible for any claims, damages, or liability associated with any other party's interpretations of the subsurface data or with reuse of the subsurface data in this report.



Appendix A
IMPORTANT INFORMATION ABOUT THIS GEOTECHNICAL-ENGINEERING REPORT

Important Information about This Geotechnical-Engineering Report

Subsurface problems are a principal cause of construction delays, cost overruns, claims, and disputes.

While you cannot eliminate all such risks, you can manage them. The following information is provided to help.

The Geoprofessional Business Association (GBA) has prepared this advisory to help you – assumedly a client representative – interpret and apply this geotechnical-engineering report as effectively as possible. In that way, you can benefit from a lowered exposure to problems associated with subsurface conditions at project sites and development of them that, for decades, have been a principal cause of construction delays, cost overruns, claims, and disputes. If you have questions or want more information about any of the issues discussed herein, contact your GBA-member geotechnical engineer. Active engagement in GBA exposes geotechnical engineers to a wide array of risk-confrontation techniques that can be of genuine benefit for everyone involved with a construction project.

Understand the Geotechnical-Engineering Services Provided for this Report

Geotechnical-engineering services typically include the planning, collection, interpretation, and analysis of exploratory data from widely spaced borings and/or test pits. Field data are combined with results from laboratory tests of soil and rock samples obtained from field exploration (if applicable), observations made during site reconnaissance, and historical information to form one or more models of the expected subsurface conditions beneath the site. Local geology and alterations of the site surface and subsurface by previous and proposed construction are also important considerations. Geotechnical engineers apply their engineering training, experience, and judgment to adapt the requirements of the prospective project to the subsurface model(s). Estimates are made of the subsurface conditions that will likely be exposed during construction as well as the expected performance of foundations and other structures being planned and/or affected by construction activities.

The culmination of these geotechnical-engineering services is typically a geotechnical-engineering report providing the data obtained, a discussion of the subsurface model(s), the engineering and geologic engineering assessments and analyses made, and the recommendations developed to satisfy the given requirements of the project. These reports may be titled investigations, explorations, studies, assessments, or evaluations. Regardless of the title used, the geotechnical-engineering report is an engineering interpretation of the subsurface conditions within the context of the project and does not represent a close examination, systematic inquiry, or thorough investigation of all site and subsurface conditions.

Geotechnical-Engineering Services are Performed for Specific Purposes, Persons, and Projects, and At Specific Times

Geotechnical engineers structure their services to meet the specific needs, goals, and risk management preferences of their clients. A geotechnical-engineering study conducted for a given civil engineer

will not likely meet the needs of a civil-works constructor or even a different civil engineer. Because each geotechnical-engineering study is unique, each geotechnical-engineering report is unique, prepared *solely* for the client.

Likewise, geotechnical-engineering services are performed for a specific project and purpose. For example, it is unlikely that a geotechnical-engineering study for a refrigerated warehouse will be the same as one prepared for a parking garage; and a few borings drilled during a preliminary study to evaluate site feasibility will not be adequate to develop geotechnical design recommendations for the project.

Do not rely on this report if your geotechnical engineer prepared it:

- for a different client;
- for a different project or purpose;
- for a different site (that may or may not include all or a portion of the original site); or
- before important events occurred at the site or adjacent to it; e.g., man-made events like construction or environmental remediation, or natural events like floods, droughts, earthquakes, or groundwater fluctuations.

Note, too, the reliability of a geotechnical-engineering report can be affected by the passage of time, because of factors like changed subsurface conditions; new or modified codes, standards, or regulations; or new techniques or tools. *If you are the least bit uncertain about the continued reliability of this report, contact your geotechnical engineer before applying the recommendations in it. A minor amount of additional testing or analysis after the passage of time – if any is required at all – could prevent major problems.*

Read this Report in Full

Costly problems have occurred because those relying on a geotechnical-engineering report did not read the report in its entirety. Do not rely on an executive summary. Do not read selective elements only. *Read and refer to the report in full.*

You Need to Inform Your Geotechnical Engineer About Change

Your geotechnical engineer considered unique, project-specific factors when developing the scope of study behind this report and developing the confirmation-dependent recommendations the report conveys. Typical changes that could erode the reliability of this report include those that affect:

- the site's size or shape;
- the elevation, configuration, location, orientation, function or weight of the proposed structure and the desired performance criteria;
- the composition of the design team; or
- project ownership.

As a general rule, *always* inform your geotechnical engineer of project or site changes – even minor ones – and request an assessment of their impact. *The geotechnical engineer who prepared this report cannot accept*

responsibility or liability for problems that arise because the geotechnical engineer was not informed about developments the engineer otherwise would have considered.

Most of the “Findings” Related in This Report Are Professional Opinions

Before construction begins, geotechnical engineers explore a site’s subsurface using various sampling and testing procedures. *Geotechnical engineers can observe actual subsurface conditions only at those specific locations where sampling and testing is performed.* The data derived from that sampling and testing were reviewed by your geotechnical engineer, who then applied professional judgement to form opinions about subsurface conditions throughout the site. Actual site-wide subsurface conditions may differ – maybe significantly – from those indicated in this report. Confront that risk by retaining your geotechnical engineer to serve on the design team through project completion to obtain informed guidance quickly, whenever needed.

This Report’s Recommendations Are Confirmation-Dependent

The recommendations included in this report – including any options or alternatives – are confirmation-dependent. In other words, they are not final, because the geotechnical engineer who developed them relied heavily on judgement and opinion to do so. Your geotechnical engineer can finalize the recommendations *only after observing actual subsurface conditions* exposed during construction. If through observation your geotechnical engineer confirms that the conditions assumed to exist actually do exist, the recommendations can be relied upon, assuming no other changes have occurred. *The geotechnical engineer who prepared this report cannot assume responsibility or liability for confirmation-dependent recommendations if you fail to retain that engineer to perform construction observation.*

This Report Could Be Misinterpreted

Other design professionals’ misinterpretation of geotechnical-engineering reports has resulted in costly problems. Confront that risk by having your geotechnical engineer serve as a continuing member of the design team, to:

- confer with other design-team members;
- help develop specifications;
- review pertinent elements of other design professionals’ plans and specifications; and
- be available whenever geotechnical-engineering guidance is needed.

You should also confront the risk of constructors misinterpreting this report. Do so by retaining your geotechnical engineer to participate in prebid and preconstruction conferences and to perform construction-phase observations.

Give Constructors a Complete Report and Guidance

Some owners and design professionals mistakenly believe they can shift unanticipated-subsurface-conditions liability to constructors by limiting the information they provide for bid preparation. To help prevent the costly, contentious problems this practice has caused, include the complete geotechnical-engineering report, along with any attachments or appendices, with your contract documents, *but be certain to note*

conspicuously that you’ve included the material for information purposes only. To avoid misunderstanding, you may also want to note that “informational purposes” means constructors have no right to rely on the interpretations, opinions, conclusions, or recommendations in the report. Be certain that constructors know they may learn about specific project requirements, including options selected from the report, *only* from the design drawings and specifications. Remind constructors that they may perform their own studies if they want to, and *be sure to allow enough time* to permit them to do so. Only then might you be in a position to give constructors the information available to you, while requiring them to at least share some of the financial responsibilities stemming from unanticipated conditions. Conducting prebid and preconstruction conferences can also be valuable in this respect.

Read Responsibility Provisions Closely

Some client representatives, design professionals, and constructors do not realize that geotechnical engineering is far less exact than other engineering disciplines. This happens in part because soil and rock on project sites are typically heterogeneous and not manufactured materials with well-defined engineering properties like steel and concrete. That lack of understanding has nurtured unrealistic expectations that have resulted in disappointments, delays, cost overruns, claims, and disputes. To confront that risk, geotechnical engineers commonly include explanatory provisions in their reports. Sometimes labeled “limitations,” many of these provisions indicate where geotechnical engineers’ responsibilities begin and end, to help others recognize their own responsibilities and risks. *Read these provisions closely.* Ask questions. Your geotechnical engineer should respond fully and frankly.

Geoenvironmental Concerns Are Not Covered

The personnel, equipment, and techniques used to perform an environmental study – e.g., a “phase-one” or “phase-two” environmental site assessment – differ significantly from those used to perform a geotechnical-engineering study. For that reason, a geotechnical-engineering report does not usually provide environmental findings, conclusions, or recommendations; e.g., about the likelihood of encountering underground storage tanks or regulated contaminants. *Unanticipated subsurface environmental problems have led to project failures.* If you have not obtained your own environmental information about the project site, ask your geotechnical consultant for a recommendation on how to find environmental risk-management guidance.

Obtain Professional Assistance to Deal with Moisture Infiltration and Mold

While your geotechnical engineer may have addressed groundwater, water infiltration, or similar issues in this report, the engineer’s services were not designed, conducted, or intended to prevent migration of moisture – including water vapor – from the soil through building slabs and walls and into the building interior, where it can cause mold growth and material-performance deficiencies. Accordingly, *proper implementation of the geotechnical engineer’s recommendations will not of itself be sufficient to prevent moisture infiltration.* Confront the risk of moisture infiltration by including building-envelope or mold specialists on the design team. *Geotechnical engineers are not building-envelope or mold specialists.*



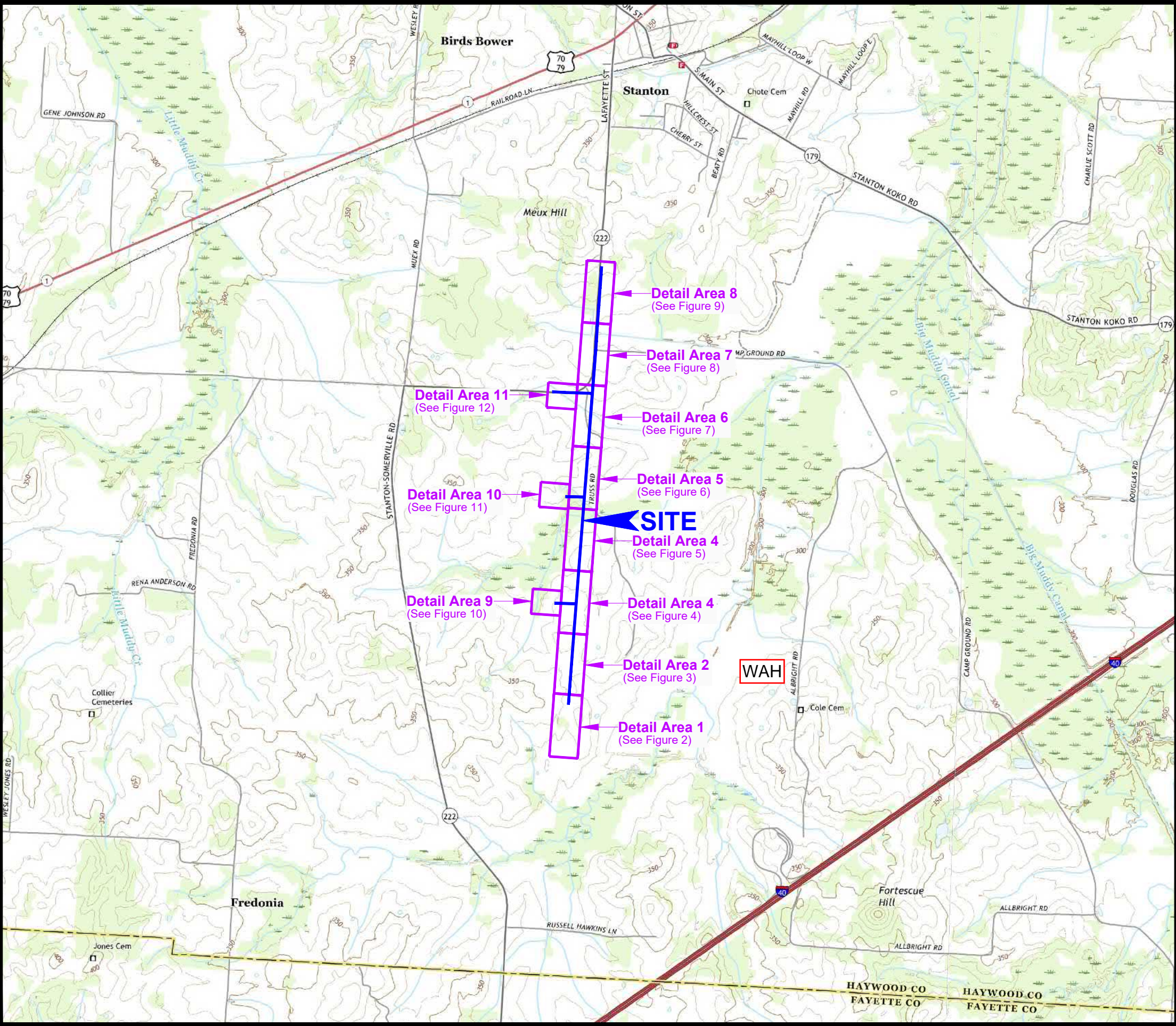
**GEOPROFESSIONAL
BUSINESS
ASSOCIATION**

Telephone: 301/565-2733

e-mail: info@geoprofessional.org www.geoprofessional.org

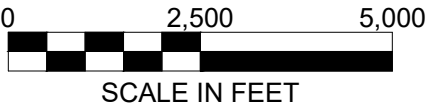



Appendix B
FIGURES AND BORING LOCATION SUMMARY

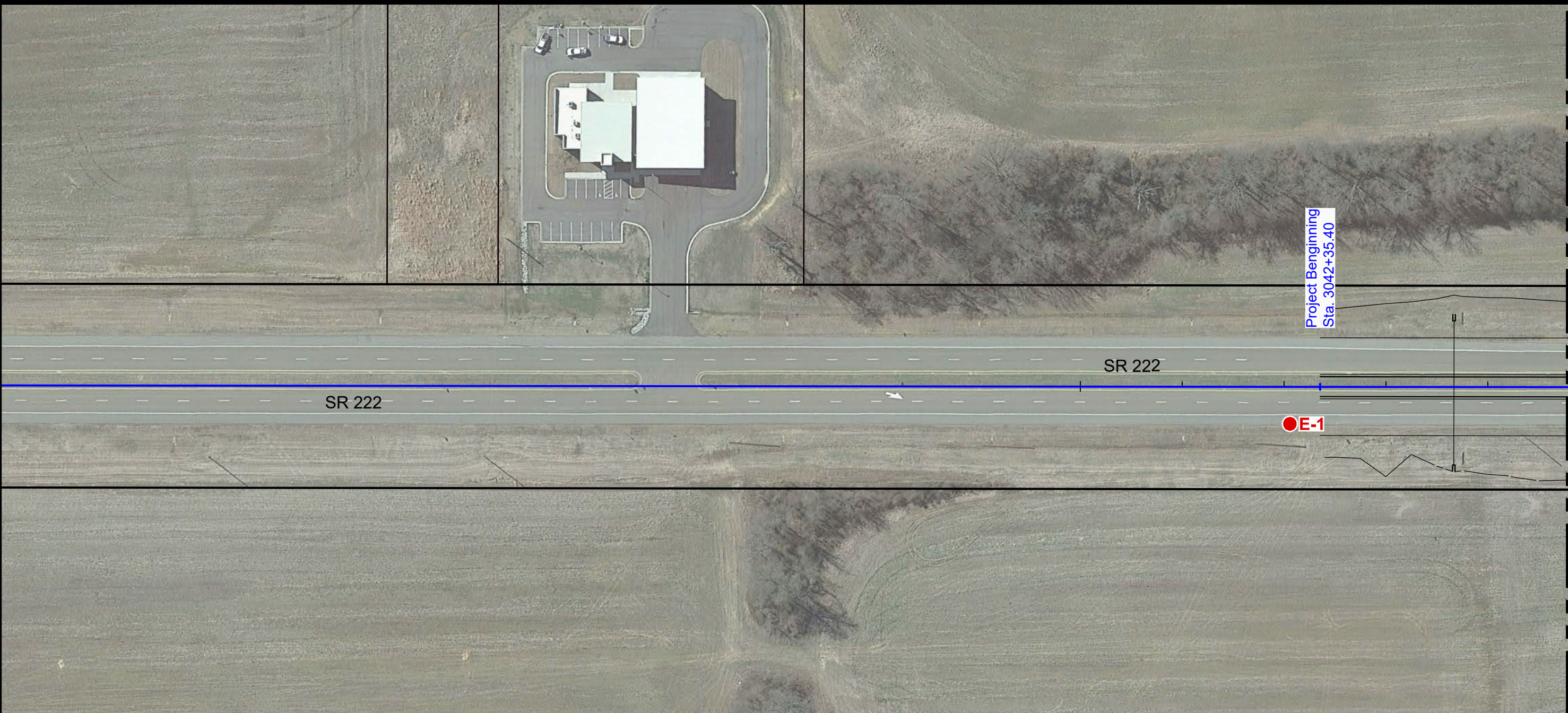


NOTES

1. Plan adapted from 7.5 minute U.S.G.S. maps for Stanton and Dancyville, Tennessee quadrangles, last revised in 2019.



Drawn By: WAH	Ck'd By: ABM	App'vd By: DBA
Date: 2-20-23	Date: 2-22-23	Date: 2-22-23
 SR-22 from Near SR-468 to Near Campground Road Haywood County, Tennessee SITE LOCATION AND TOPOGRAPHY		
Project Number J042140.01		FIGURE 1



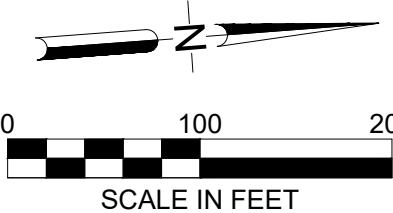
MATCH LINE - FIGURE 3


NOTES

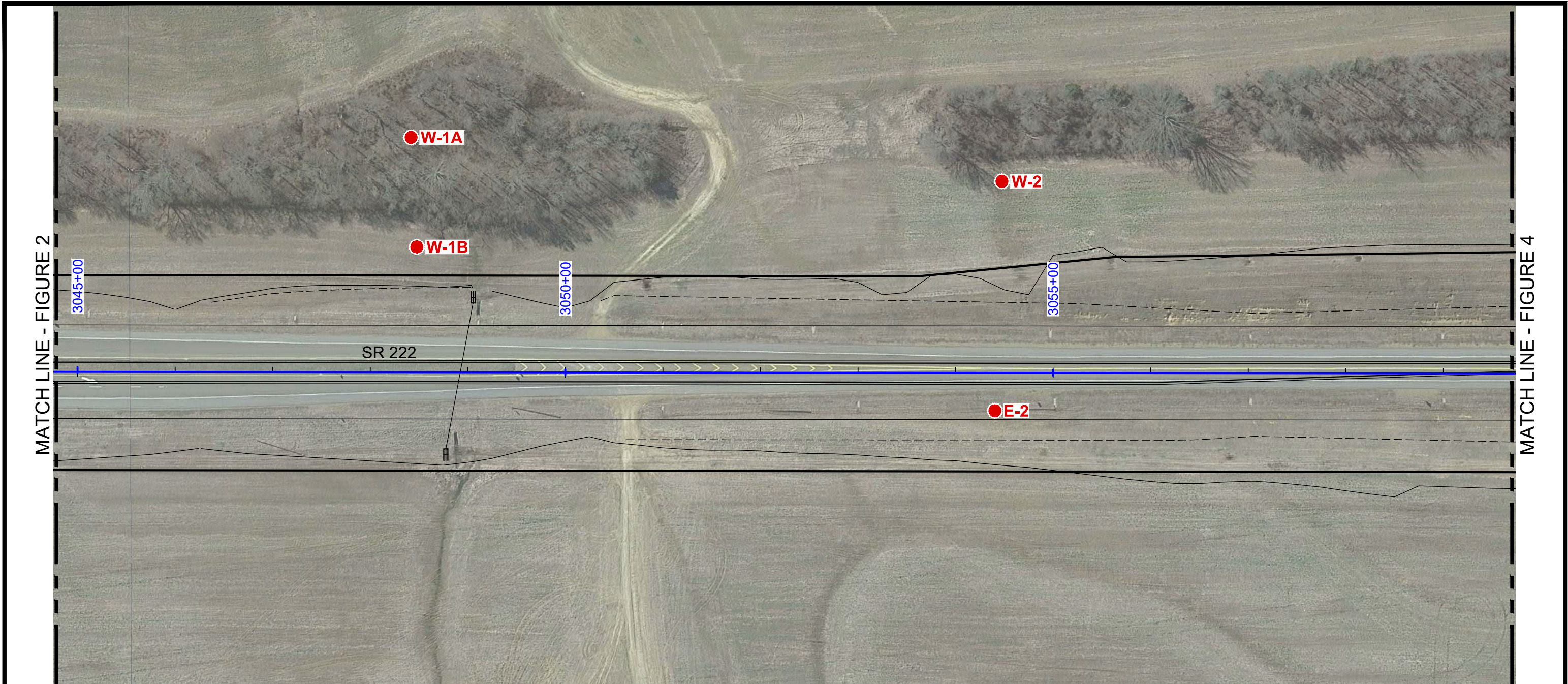
1. Plan adapted from a February 2022 aerial photograph courtesy of Google Earth and drawings dated February 9, 2023, titled "Proposed Layout", prepared by State of Tennessee Department of Transportation.
2. Borings were located in the field by the project surveyor.

LEGEND

● Boring Location



Drawn By: WAH	Ck'd By: ABM	App'vd By: DBA
Date: 2-20-23	Date: 2-22-23	Date: 2-22-23
		
SR-222 from Near SR-468 to Near Campground Road Haywood County, Tennessee		
AERIAL PHOTOGRAPH OF DETAIL AREA 1 AND BORING LOCATIONS		
Project Number J042140.01		FIGURE 2

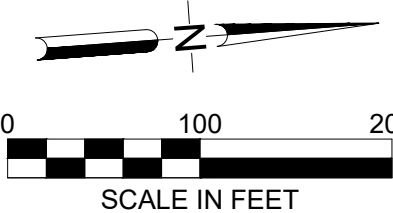


NOTES

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LEGEND

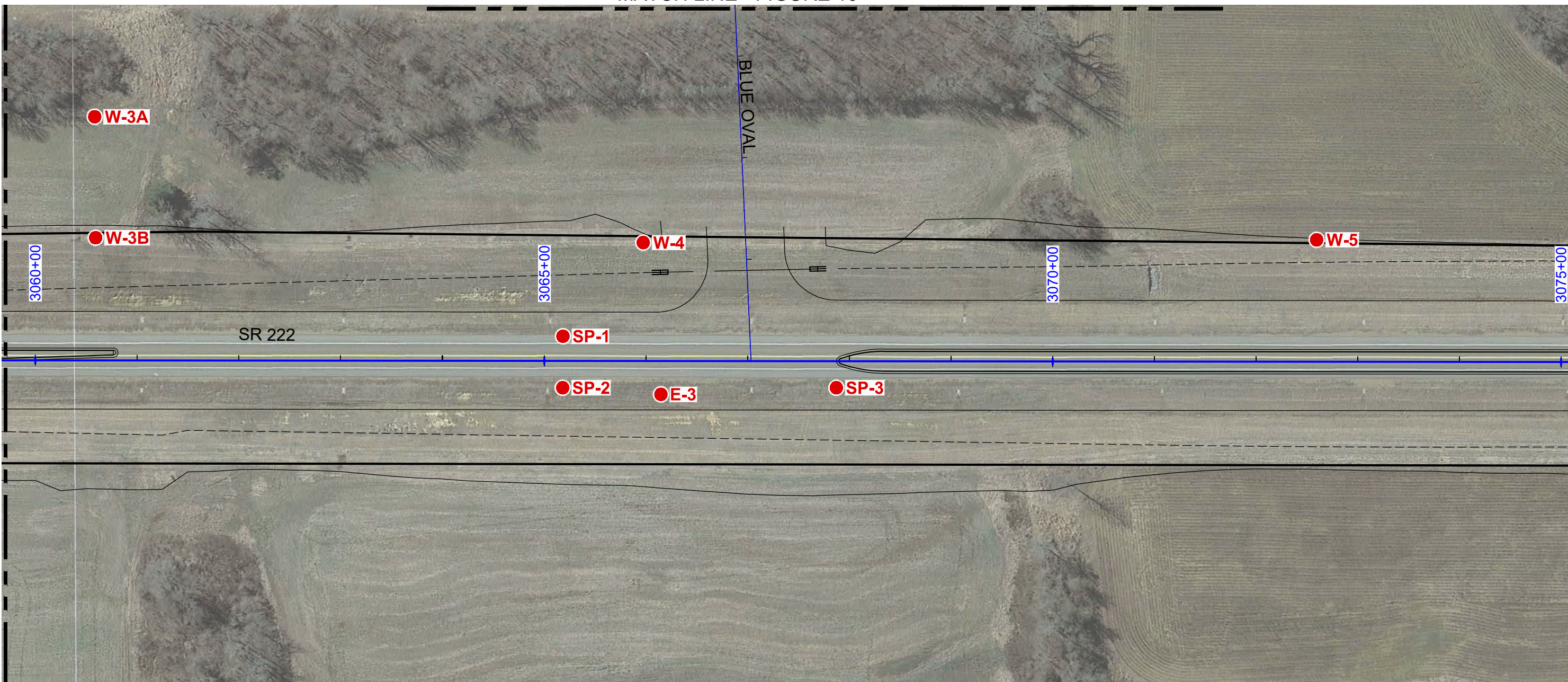
● Boring Location



Drawn By: WAH	Ck'd By: ABM	App'vd By: DBA
Date: 2-20-23	Date: 2-22-23	Date: 2-22-23
<div><div><div></div><div></div><div></div><div></div><div></div></div><div><div>GEOTECHNOLOGY</div><div>A Universal Engineering Sciences Company</div></div></div>		
SR-222 from Near SR-468 to Near Campground Road Haywood County, Tennessee		
AERIAL PHOTOGRAPH OF DETAIL AREA 2 AND BORING LOCATIONS		
Project Number J042140.01		FIGURE 3

MATCH LINE - FIGURE 10

MATCH LINE - FIGURE 3



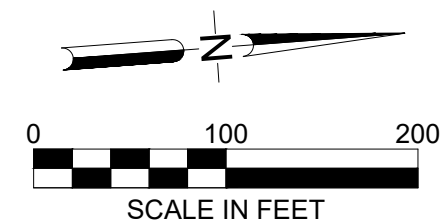
MATCH LINE - FIGURE 5

NOTES

1. Plan adapted from a February 2022 aerial photograph courtesy of Google Earth and drawings dated February 9, 2023, titled "Proposed Layout", prepared by State of Tennessee Department of Transportation.
2. Borings were located in the field by the project surveyor.

LEGEND

- Boring Location



Drawn By: WAH	Ck'd By: ABM	App'd By: DBA
Date: 2-20-23	Date: 2-22-23	Date: 2-22-23

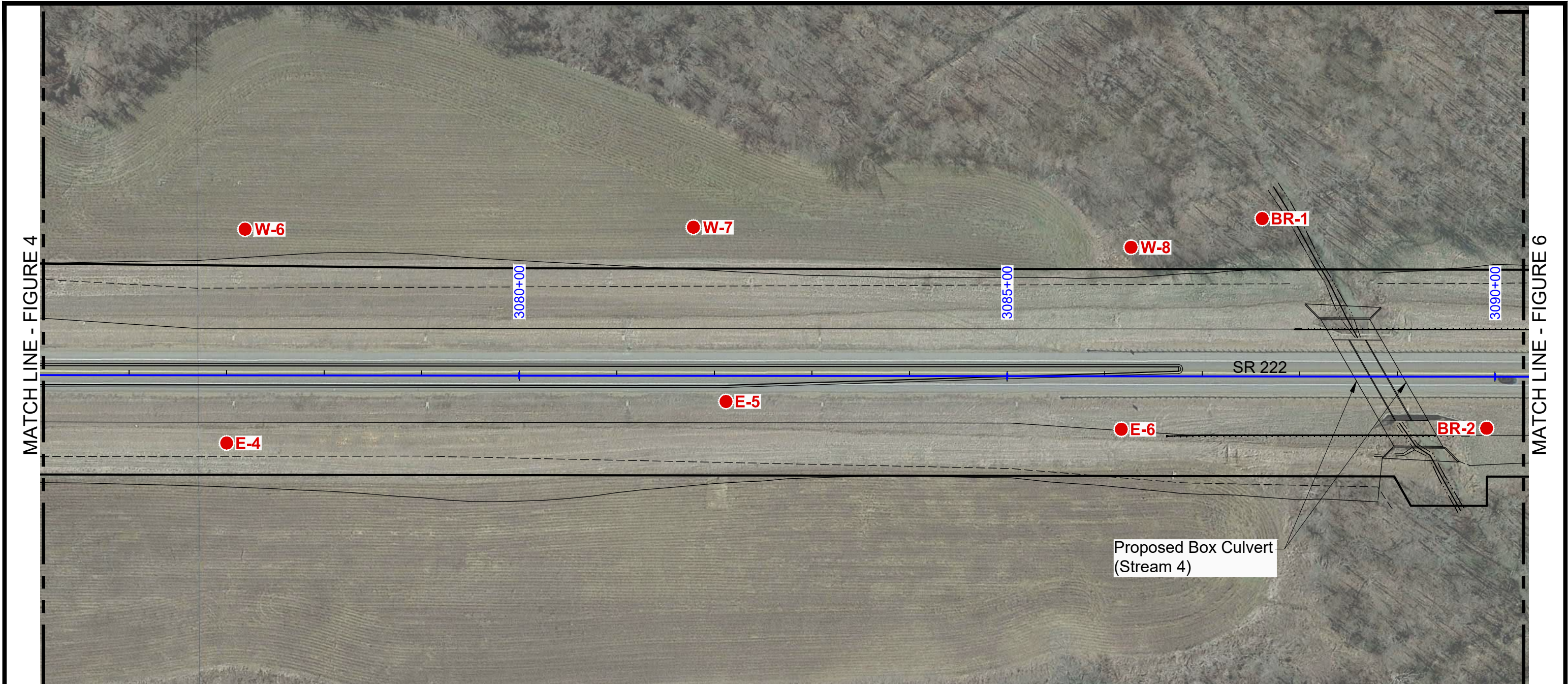


SR-222 from Near SR-468
to Near Campground Road
Haywood County, Tennessee

AERIAL PHOTOGRAPH OF DETAIL AREA 3 AND BORING LOCATIONS

Project Number
J042140.01

FIGURE 4

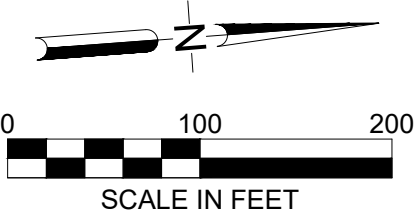



NOTES

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- 2. Borings were located in the field by the project surveyor.

LEGEND

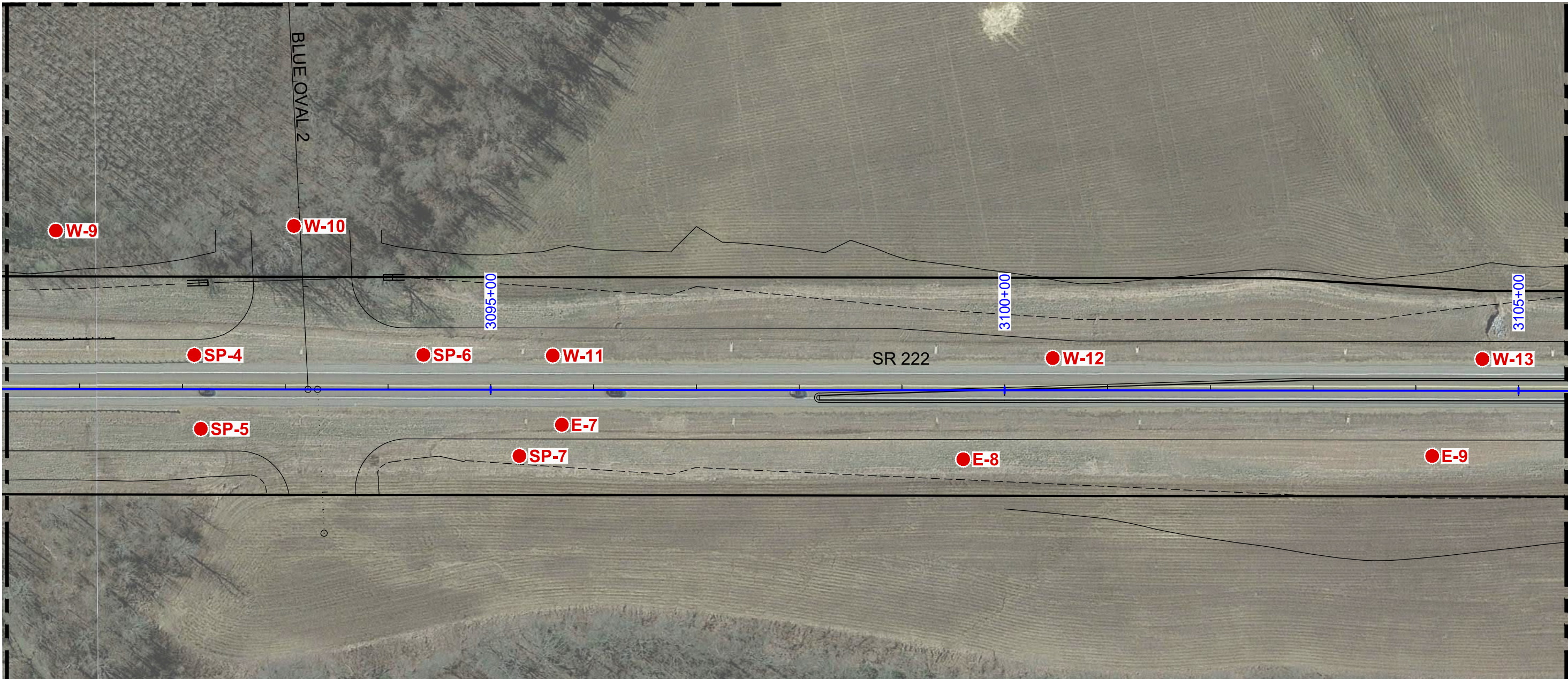
● Boring Location



Drawn By: WAH	Ck'd By: ABM	App'vd By: DBA
Date: 2-20-23	Date: 2-22-23	Date: 2-22-23
<div>GEOTECHNOLOGY <small>A Universal Engineering Sciences Company</small></div>		
SR-222 from Near SR-468 to Near Campground Road Haywood County, Tennessee		
AERIAL PHOTOGRAPH OF DETAIL AREA 4 AND BORING LOCATIONS		
Project Number J042140.01		FIGURE 5

MATCH LINE - FIGURE 11

MATCH LINE - FIGURE 5



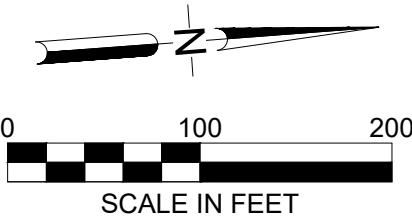
MATCH LINE - FIGURE 7


NOTES

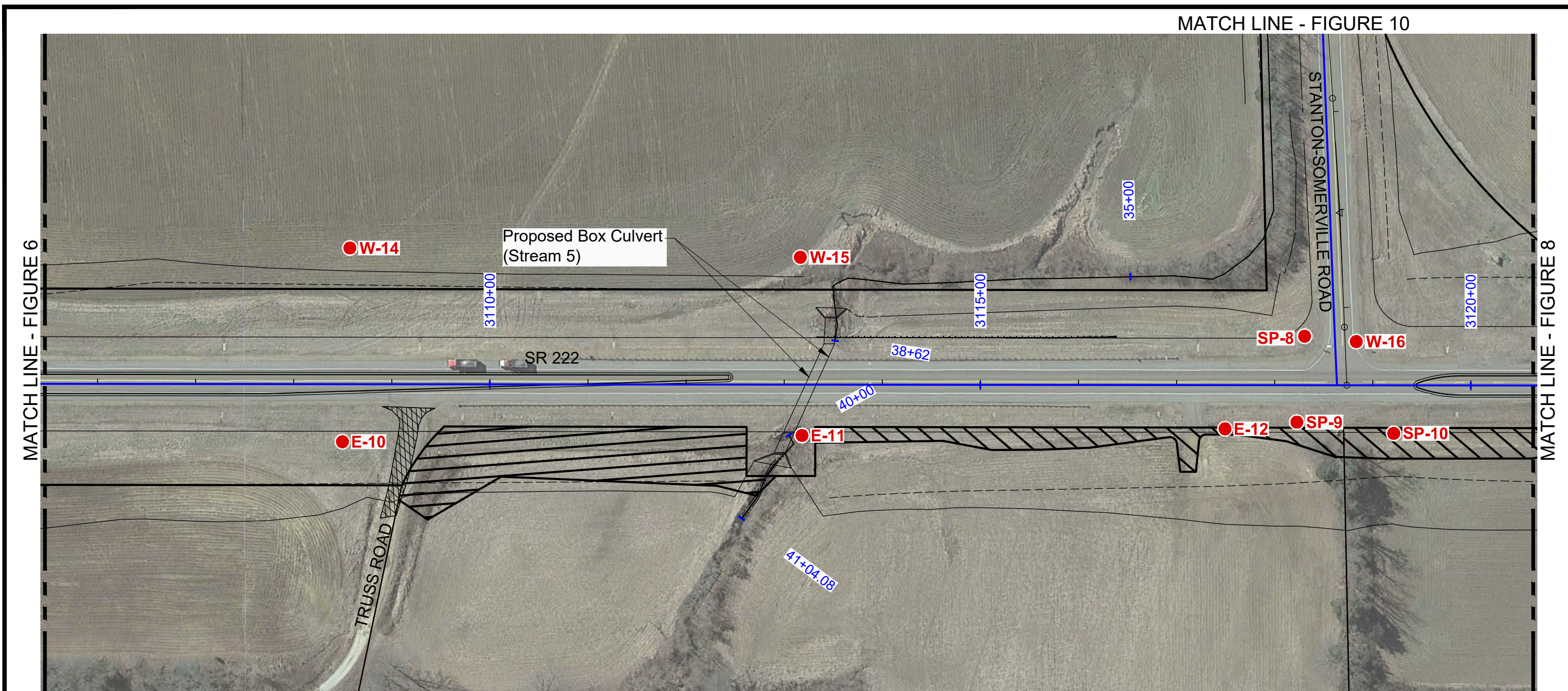
1. Plan adapted from a February 2022 aerial photograph courtesy of Google Earth and drawings dated February 9, 2023, titled "Proposed Layout", prepared by State of Tennessee Department of Transportation.
2. Borings were located in the field by the project surveyor.

LEGEND

● Boring Location



Drawn By: WAH	Ck'd By: ABM	App'vd By: DBA
Date: 2-20-23	Date: 2-22-23	Date: 2-22-23
		
SR-222 from Near SR-468 to Near Campground Road Haywood County, Tennessee		
AERIAL PHOTOGRAPH OF DETAIL AREA 5 AND BORING LOCATIONS		
Project Number J042140.01		FIGURE 6

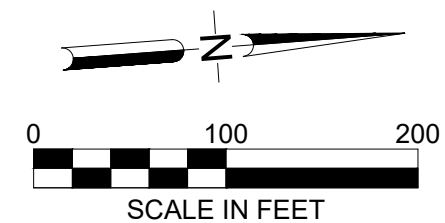



NOTES

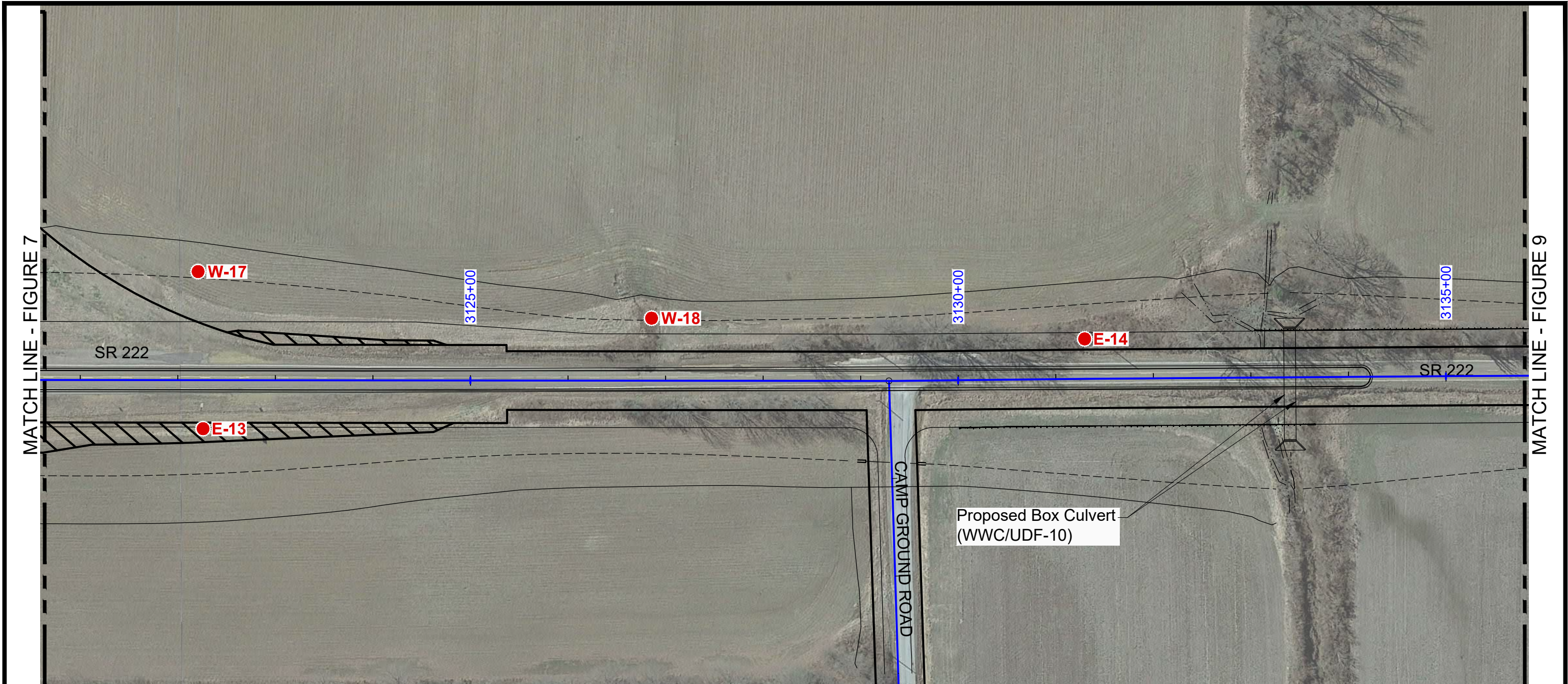
1. Plan adapted from a February 2022 aerial photograph courtesy of Google Earth and drawings dated February 9, 2023, titled "Proposed Layout", prepared by State of Tennessee Department of Transportation.
2. Borings were located in the field by the project surveyor.

LEGEND

- Boring Location



Drawn By: WAH	Ck'd By: ABM	App'd By: DBA
Date: 2-20-23	Date: 2-22-23	Date: 2-22-23
 GEOTECHNOLOGY A Universal Engineering Sciences Company		
SR-222 from Near SR-468 to Near Campground Road Haywood County, Tennessee		
AERIAL PHOTOGRAPH OF DETAIL AREA 6 AND BORING LOCATIONS		
Project Number J042140.01		FIGURE 7

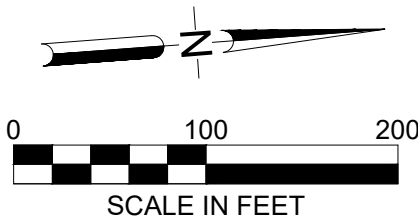



NOTES

1. Plan adapted from a February 2022 aerial photograph courtesy of Google Earth and drawings dated February 9, 2023, titled "Proposed Layout", prepared by State of Tennessee Department of Transportation.
2. Borings were located in the field by the project surveyor.

LEGEND

● Boring Location



Drawn By: WAH	Ck'd By: ABM	App'vd By: DBA
Date: 2-20-23	Date: 2-22-23	Date: 2-22-23
		
SR-222 from Near SR-468 to Near Campground Road Haywood County, Tennessee		
AERIAL PHOTOGRAPH OF DETAIL AREA 7 AND BORING LOCATIONS		
Project Number J042140.01		FIGURE 8

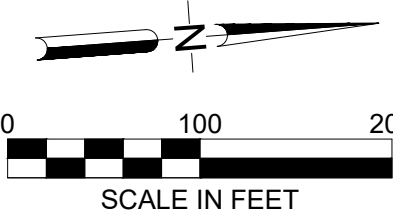



NOTES

1. Plan adapted from a February 2022 aerial photograph courtesy of Google Earth and drawings dated February 9, 2023, titled "Proposed Layout", prepared by State of Tennessee Department of Transportation.
2. Borings were located in the field by the project surveyor.

LEGEND

● Boring Location



Drawn By: WAH	Ck'd By: ABM	App'vd By: DBA
Date: 2-20-23	Date: 2-22-23	Date: 2-22-23
 A Universal Engineering Sciences Company		
SR-222 from Near SR-468 to Near Campground Road Haywood County, Tennessee		
AERIAL PHOTOGRAPH OF DETAIL AREA 8 AND BORING LOCATIONS		
Project Number J042140.01		FIGURE 9



MATCH LINE - FIGURE 4

NOTES

1. Plan adapted from a February 2022 aerial photograph courtesy of Google Earth and drawings dated February 9, 2023, titled "Proposed Layout", prepared by State of Tennessee Department of Transportation.
2. Borings were located in the field by the project surveyor.

LEGEND

● Boring Location



Drawn By: WAH	Ck'd By: ABM	App'vd By: DBA
Date: 2-20-23	Date: 2-22-23	Date: 2-22-23

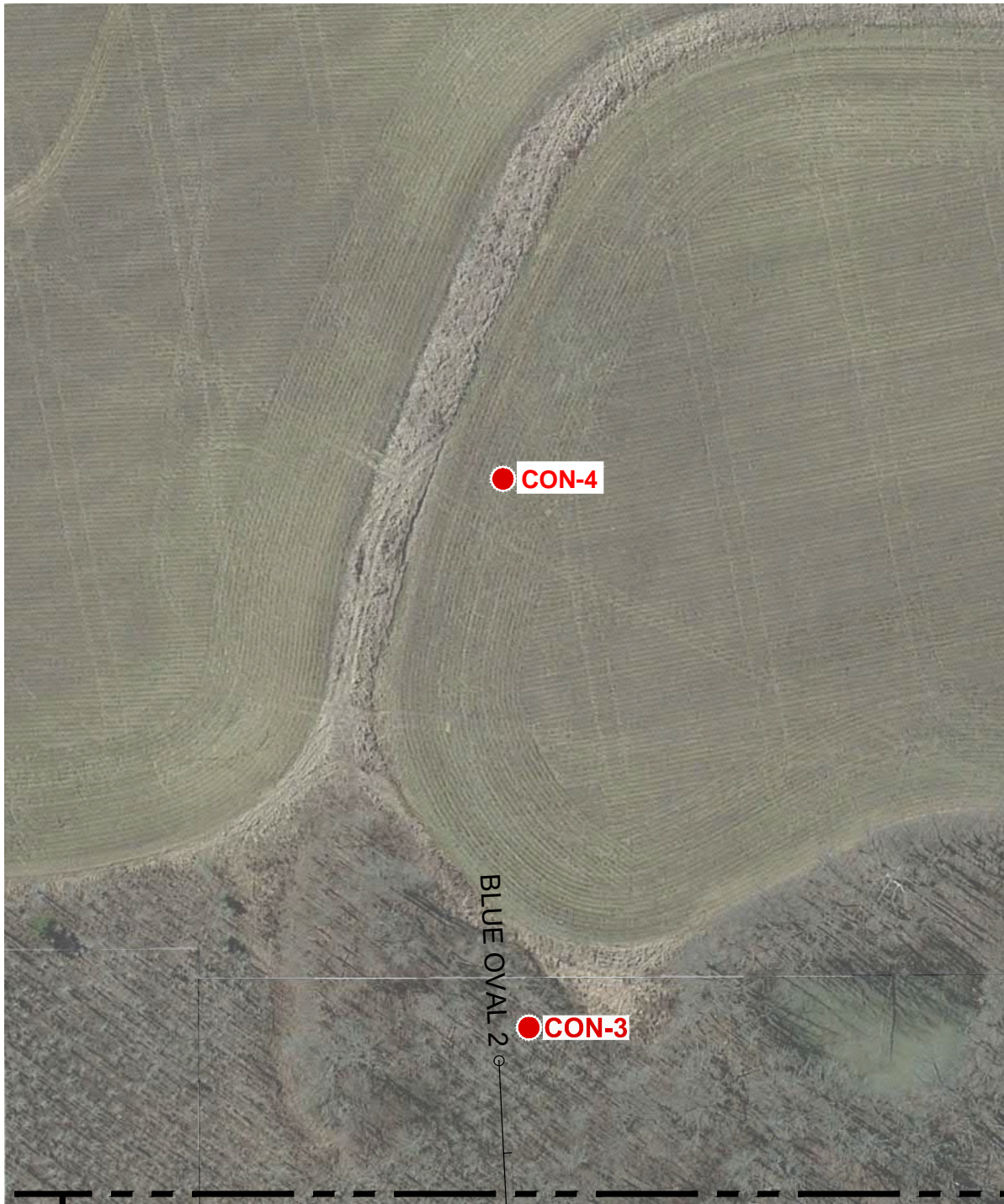


SR-222 from Near SR-468
to Near Campground Road
Haywood County, Tennessee

AERIAL PHOTOGRAPH OF DETAIL AREA 9 AND BORING LOCATIONS

Project Number
J042140.01

FIGURE 10



MATCH LINE - FIGURE 6

NOTES

1. Plan adapted from a February 2022 aerial photograph courtesy of Google Earth and drawings dated February 9, 2023, titled "Proposed Layout", prepared by State of Tennessee Department of Transportation.
2. Borings were located in the field by the project surveyor.

LEGEND

● Boring Location



Drawn By: WAH	Ck'd By: ABM	App'vd By: DBA
Date: 2-20-23	Date: 2-22-23	Date: 2-22-23



SR-222 from Near SR-468
to Near Campground Road
Haywood County, Tennessee

AERIAL PHOTOGRAPH OF DETAIL AREA 10 AND BORING LOCATIONS

Project Number
J042140.01

FIGURE 11



MATCH LINE - FIGURE 7

NOTES

1. Plan adapted from a February 2022 aerial photograph courtesy of Google Earth and drawings dated February 9, 2023, titled "Proposed Layout", prepared by State of Tennessee Department of Transportation.
2. Borings were located in the field by the project surveyor.

LEGEND

● Boring Location



Drawn By: WAH	Ck'd By: ABM	App'vd By: DBA
Date: 2-20-23	Date: 2-22-23	Date: 2-22-23



SR-222 from Near SR-468
to Near Campground Road
Haywood County, Tennessee

AERIAL PHOTOGRAPH OF DETAIL AREA 11 AND BORING LOCATIONS

Project Number
J042140.01

FIGURE 12

Boring No.	Location				Elevation (feet)	Termination Depth (feet)
	SR-222 Station	Offset	Northing	Easting		
E-1	3042+05.23	36.35	412743.98	953613.52	340.4	15
W-1A	3048+41.09	-240.63	413399.22	953386.17	340.7	30
W-1B	3048+47.07	-128.4	413396.57	953498.53	333.5	15
E-2	3054+39.80	38.79	413974.72	953710.73	329.2	15
W-2	3054+46.81	-196.29	413999.75	953476.88	337.4	30
W-3A	3060+57.54	-239.43	414611.99	953480.75	342.4	30
W-3B	3060+58.57	-120.55	414603.89	953599.36	342.7	15
SP-2	3065+18.09	26.38	415050.77	953781.13	326.0	25
SP-1	3065+18.28	-24.23	415054.85	953730.69	326.0	25
W-4	3065+97.13	-116.34	415140.54	953644.90	329.3	15
CON-2	3066+00.74	-610.05	415182.04	953152.93	326.5	15
E-3	3066+14.72	32.75	415146.63	953794.90	324.7	15
CON-1	3067+61.44	-405.91	415326.59	953368.80	331.8	15
SP-3	3067+87.25	26.1	415319.16	953801.51	325.5	25
W-5	3072+59.43	-119.81	415801.15	953692.29	323.6	15
E-4	3077+00.09	69.38	416225.99	953914.75	317.8	15
W-6	3077+18.72	-149.75	416261.38	953697.70	322.1	15
W-7	3081+78.25	-152.27	416719.75	953730.45	313.4	15
E-5	3082+11.87	26.23	416739.57	953911.01	319.6	15
E-6	3086+17.06	54.29	417141.41	953970.10	311.9	15
W-8	3086+26.83	-132.23	417165.47	953784.87	309.1	15
BR-1	3087+61.24	-161.79	417301.75	953765.72	308.7	75*
BR-2	3089+91.55	52.8	417514.91	953997.36	309.7	80
W-9	3090+76.81	-154.16	417615.81	953797.55	309.1	15
SP-4	3092+11.61	-33.33	417740.93	953928.37	314.2	25
SP-5	3092+18.06	38.45	417741.86	954000.44	314.1	25
CON-4	3092+85.00	-842.93	417876.25	953126.80	326.8	15
W-10	3093+08.42	-158.95	417847.10	953810.56	320.0	15
CON-3	3093+17.49	-477.24	417880.57	953493.91	321.8	15
SP-6	3094+34.48	-33.69	417963.17	953945.12	316.2	25
SP-7	3095+28.03	64.48	418048.91	954050.19	316.0	25
W-11	3095+60.34	-33.22	418088.63	953955.26	316.2	25
E-7	3095+69.27	34.1	418092.36	954023.06	317.4	15
E-8	3099+59.81	67.19	418479.21	954086.03	321.2	15
W-12	3100+46.79	-31.29	418573.49	953994.52	319.5	15
E-9	3104+16.03	63.52	418934.37	954117.40	325.3	15
W-13	3104+64.77	-30.81	418990.20	954027.09	321.0	15
E-10	3108+49.86	58.63	419367.29	954145.83	315.1	15
W-14	3108+57.23	-138.86	419389.80	953949.49	314.2	15
W-15	3113+16.42	-129.95	419846.95	953993.62	311.6	15
E-11	3113+18.31	51.77	419834.88	954174.95	311.5	15
E-12	3117+49.53	44.55	420265.39	954200.85	317.3	15
CON-7	3118+08.95	-1055.54	420409.08	953108.57	318.3	15
SP-9	3118+22.73	37.63	420338.90	954199.58	320.0	25
CON-6	3118+28.13	-734.39	420403.55	953430.25	319.3	15
SP-8	3118+30.52	-49.98	420353.39	954112.82	319.8	25
CON-5	3118+52.27	-435.47	420404.67	953730.14	320.3	15
W-16	3118+83.21	-44.6	420405.52	954122.23	321.1	15

*Refusal encountered

Boring No.	Location				Elevation (feet)	Termination Depth (feet)
	SR-222 Station	Offset	Northing	Easting		
SP-10	3119+21.47	48.98	420436.47	954218.47	319.0	25
W-17	3122+20.82	-111.34	420747.25	954081.60	320.9	15
E-13	3122+26.10	49.68	420740.15	954242.55	319.2	15
W-18	3126+85.69	-64.07	421207.12	954164.42	315.7	15
E-14	3131+29.98	-40.95	421648.15	954219.17	311.7	15
W-19	3136+44.65	-71.41	422163.77	954224.16	313.2	15
E-15	3139+41.54	24.49	422453.10	954340.86	314.9	15
W-20	3139+47.51	-82.06	422467.08	954235.06	315.9	15
W-21	3143+29.78	-83.69	422848.38	954262.24	326.5	15
E-16	3143+37.91	20.32	422848.66	954366.57	318.1	15



Appendix C
BORING INFORMATION

NOTE: STRATIFICATION LINES REPRESENT THE APPROXIMATE BOUNDARIES BETWEEN SOIL TYPES
 LOG OF BORING 2020 JDM - ELEVATIONS J042140.01 GINT.GPJ GTINC 0638301.GPJ 2/2/23 THE TRANSITION MAY BE GRADUAL. GRAPHIC LOG FOR ILLUSTRATION PURPOSES ONLY.

Surface Elevation: <u>340.7</u>		Completion Date: <u>12/27/23</u>		GRAPHIC LOG	DRY UNIT WEIGHT (pcf) SPT BLOW COUNTS CORE RECOVERY/RQD	SAMPLES	SHEAR STRENGTH, tsf				
Datum <u>NAD83</u>		Station: <u>3048+41.1</u>					Δ - UU/2	○ - QU/2	□ - SV		
		Offset: <u>-240.6</u>					0.5	1.0	1.5	2.0	2.5
							STANDARD PENETRATION RESISTANCE (ASTM D 1586)				
DEPTH IN FEET	ELEVATION IN FEET	DESCRIPTION OF MATERIAL	▲ N-VALUE (BLOWS PER FOOT)								
			WATER CONTENT, %								
				PL	10	20	30	40	50	LL	
		Topsoil: 6 inches									
		Medium stiff to stiff, gray, silty, LEAN CLAY - CL									
			2-3-4	SS1							
			3-4-5	SS2							
5	336										
		Medium stiff to stiff, gray, FAT CLAY - (CH)									
			2-3-3	SS3							
			102	ST4							
10	331										
		Medium stiff to stiff, brown and gray, sandy, LEAN CLAY, trace organic - (CL)									
			2-3-4	SS5							
15	326										
			4-3-5	SS6							
20	321										
		69% passing No. 200 sieve									
			2-2-3	SS7							
25	316										
			3-5-6	SS8							
30	311	Boring terminated at 30 feet.									

GROUNDWATER DATA

X FREE WATER NOT ENCOUNTERED DURING DRILLING

DRILLING DATA

___ AUGER 3 3/4" HOLLOW STEM WASHBORING FROM ___ FEET

KJB DRILLER GBB LOGGER

CME 750X DRILL RIG


HAMMER TYPE Auto

HAMMER EFFICIENCY 84 %

Drawn by: NMRG Checked by: ABM App'vd. by: DBA

Date: 1/5/23 Date: 2/20/23 Date: 2/20/23

REMARKS:



SR-222
 From Near SR-468 To Near Campground Rd
 Haywood County, Tennessee

LOG OF BORING: W- 1A

Project No. J042140.01

NOTE: STRATIFICATION LINES REPRESENT THE APPROXIMATE BOUNDARIES BETWEEN SOIL TYPES
 LOG OF BORING 2020 JDM - ELEVATIONS J042140.01 GINT.GPJ GTINC 0638301.GPJ 2/20/23 THE TRANSITION MAY BE GRADUAL. GRAPHIC LOG FOR ILLUSTRATION PURPOSES ONLY.

Surface Elevation: <u>333.5</u>		Completion Date: <u>12/22/22</u>		GRAPHIC LOG	DRY UNIT WEIGHT (pcf) SPT BLOW COUNTS CORE RECOVERY/RQD	SAMPLES	SHEAR STRENGTH, tsf		
Datum <u>NAD83</u>		Station: <u>3048+47.1</u>					Δ - UU/2	○ - QU/2	□ - SV
		Offset: <u>-128.4</u>					0.5	1.0	1.5
							2.0	2.5	
DEPTH IN FEET	ELEVATION IN FEET	DESCRIPTION OF MATERIAL	STANDARD PENETRATION RESISTANCE (ASTM D 1586)						
			▲ N-VALUE (BLOWS PER FOOT)						
			PLI WATER CONTENT, % LL						
			10 20 30 40 50						
		Fill: 6 inches of gravel							
		Medium stiff to hard, brown, LEAN CLAY - (CL)							
		97% passing No. 200 sieve	6-3-3	SS1					
			118	ST2					
5	329	Medium stiff to stiff, brown to gray, clayey SILT - ML							
			5-4-4	SS3					
			4-5-9	SS4					
10	324								
		Stiff, gray to brown, silty, LEAN CLAY - CL	3-4-5	SS5					
		Boring terminated at 15 feet.							
15	319								
20	314								
25	309								
30	304								

GROUNDWATER DATA

☒ FREE WATER NOT ENCOUNTERED DURING DRILLING

DRILLING DATA

___ AUGER 3 3/4" HOLLOW STEM WASHBORING FROM ___ FEET

KJB DRILLER GBB LOGGER

CME 750X DRILL RIG

HAMMER TYPE Auto

HAMMER EFFICIENCY 84 %

Drawn by: GBB Checked by: ABM App'vd. by: DBA

Date: 1/9/23 Date: 2/20/23 Date: 2/20/23

REMARKS:

GEOTECHNOLOGY
A Universal Engineering Sciences Company

SR-222
From Near SR-468 To Near Campground Rd
Haywood County, Tennessee


LOG OF BORING: W- 1B

Project No. J042140.01

NOTE: STRATIFICATION LINES REPRESENT THE APPROXIMATE BOUNDARIES BETWEEN SOIL TYPES
 LOG OF BORING 2020 JDM - ELEVATIONS J042140.01 GINT.GPJ GTINC 0638301.GPJ 2/2/23 THE TRANSITION MAY BE GRADUAL. GRAPHIC LOG FOR ILLUSTRATION PURPOSES ONLY.

Surface Elevation: <u>329.3</u>		Completion Date: <u>12/13/22</u>		GRAPHIC LOG	DRY UNIT WEIGHT (pcf) SPT BLOW COUNTS CORE RECOVERY/RQD	SAMPLES	SHEAR STRENGTH, tsf				
Datum <u>NAD83</u>		Station: <u>3054+39.8</u>					Δ - UU/2	○ - QU/2	□ - SV		
		Offset: <u>38.8</u>					0.5	1.0	1.5	2.0	2.5
							STANDARD PENETRATION RESISTANCE (ASTM D 1586)				
DEPTH IN FEET	ELEVATION IN FEET	DESCRIPTION OF MATERIAL	▲ N-VALUE (BLOWS PER FOOT)								
			WATER CONTENT, %								
				PL	10	20	30	40	50	LL	
		Fill: 6 inches of gravel									
		Stiff, brown and gray, silty, LEAN CLAY, trace organics - CL		3-5-6	SS1	▲	●				
				3-6-8	SS2	▲	●				
5	324	trace gravel		3-4-6	SS3	▲	●				
				2-4-6	SS4	▲	●				
10	319										
		Medium stiff, tan, gray and brown, FAT CLAY, little organics - CH		3-3-4	SS5	▲	●				
15	314	Boring terminated at 15 feet.									
20	309										
25	304										
30	299										

GROUNDWATER DATA		DRILLING DATA	
<u>X</u> FREE WATER NOT ENCOUNTERED DURING DRILLING		___ AUGER <u>3 3/4"</u> HOLLOW STEM WASHBORING FROM ___ FEET	
		<u>KJB</u> DRILLER <u>GBB</u> LOGGER	
		<u>CME 750X</u> DRILL RIG	
		HAMMER TYPE <u>Auto</u>	
		HAMMER EFFICIENCY <u>84</u> %	

Drawn by: SEM	Checked by: ABM	App'vd. by: DBA
Date: 12/21/22	Date: 2/20/23	Date: 2/20/23
		
SR-222 From Near SR-468 To Near Campground Rd Haywood County, Tennessee		
LOG OF BORING: E- 2		
Project No. J042140.01		

REMARKS:

NOTE: STRATIFICATION LINES REPRESENT THE APPROXIMATE BOUNDARIES BETWEEN SOIL TYPES
 LOG OF BORING 2020 JDM - ELEVATIONS J042140.01 GINT.GPJ GTINC 0638301.GPJ 2/2/23 THE TRANSITION MAY BE GRADUAL. GRAPHIC LOG FOR ILLUSTRATION PURPOSES ONLY.

Surface Elevation: <u>337.4</u>		Completion Date: <u>12/27/23</u>		GRAPHIC LOG	DRY UNIT WEIGHT (pcf) SPT BLOW COUNTS CORE RECOVERY/RQD	SAMPLES	SHEAR STRENGTH, tsf				
Datum <u>NAD83</u>		Station: <u>3054+46.8</u>					Δ - UU/2	○ - QU/2	□ - SV		
		Offset: <u>-196.3</u>					0.5	1.0	1.5	2.0	2.5
							STANDARD PENETRATION RESISTANCE (ASTM D 1586)				
DEPTH IN FEET	ELEVATION IN FEET	DESCRIPTION OF MATERIAL	▲ N-VALUE (BLOWS PER FOOT)								
			WATER CONTENT, %								
				PL	10	20	30	40	50	LL	
		Fill: 6 inches of gravel									
		Medium stiff to stiff, brown and gray, silty, LEAN CLAY - (CL)		2-2-4	SS1	▲		●			
				2-2-4	SS2	▲		●			
5	332			2-3-4	SS3	▲		●			
				2-3-3	SS4	▲		●			
				2-4-4	SS5	▲		●			
10	327										
15	322			98	ST6		4	●		1	
20	317										
25	312	Medium stiff to stiff, gray and brown, sandy, LEAN CLAY - CL		4-4-4	SS7	▲		●			
30	307	Boring terminated at 30 feet.		4-6-4	SS8	▲		●			

GROUNDWATER DATA

X FREE WATER NOT ENCOUNTERED DURING DRILLING

DRILLING DATA

___ AUGER 3 3/4" HOLLOW STEM WASHBORING FROM ___ FEET

KJB DRILLER GBB LOGGER

CME 750X DRILL RIG

HAMMER TYPE Auto


HAMMER EFFICIENCY 84 %

Drawn by: GBB
Date: 1/5/23

Checked by: ABM
Date: 2/20/23

App'vd. by: DBA
Date: 2/20/23

REMARKS:



SR-222
From Near SR-468 To Near Campground Rd
Haywood County, Tennessee


LOG OF BORING: W- 2


Project No. J042140.01

LOG OF BORING 2020_JDM - ELEVATIONS J042140.01 GINT.GPJ GTINC 06383031 GPJ 227498
NOTE: STRATIFICATION LINES REPRESENT THE APPROXIMATE BOUNDARIES BETWEEN SOIL TYPES
AND THE TRANSITION MAY BE GRADUAL. GRAPHIC LOG FOR ILLUSTRATION PURPOSES ONLY.

NOTE: STRATIFICATION LINES REPRESENT THE APPROXIMATE BOUNDARIES BETWEEN SOIL TYPES
 LOG OF BORING 2020 JDM - ELEVATIONS J042140.01 GINT.GPJ GTINC 0638301.GPJ 2/2/23 THE TRANSITION MAY BE GRADUAL. GRAPHIC LOG FOR ILLUSTRATION PURPOSES ONLY.

Surface Elevation: <u>326.0</u>		Completion Date: <u>1/26/23</u>		GRAPHIC LOG	DRY UNIT WEIGHT (pcf) SPT BLOW COUNTS CORE RECOVERY/RQD	SAMPLES	SHEAR STRENGTH, tsf						
Datum <u>NAD83</u>		Station: <u>3065+18.3</u>					Δ - UU/2	○ - QU/2	□ - SV				
		Offset: <u>-24.2</u>					0.5	1.0	1.5	2.0	2.5		
							STANDARD PENETRATION RESISTANCE (ASTM D 1586)						
DEPTH IN FEET	ELEVATION IN FEET	DESCRIPTION OF MATERIAL					▲ N-VALUE (BLOWS PER FOOT)						
							WATER CONTENT, %						
							PL	10	20	30	40	50	LL
		Topsoil: 6 inches											
		Stiff, tan and red, sandy, LEAN CLAY - CL			3-5-8	SS1							
		Very stiff, tan and red, sandy, FAT CLAY - (CH)			107	ST2							
5	321	Medium dense, white and pink, CLAYEY SAND - (SC)			4-6-9	SS3							
		22% passing No. 200 sieve			4-6-6	SS4							
10	316	Medium stiff to stiff, tan to white, sandy, LEAN CLAY - CL			3-3-4	SS5							
		trace organics											
15	311				5-5-5	SS6							
20	306												
		Medium dense, orange and gray, CLAYEY SAND, trace organics - SC			5-11-13	SS7							
25	301	Boring terminated at 25 feet.											
30	296												

GROUNDWATER DATA		DRILLING DATA		Drawn by: JSH	Checked by: ABM	App'vd. by: DBA
<input checked="" type="checkbox"/> FREE WATER NOT ENCOUNTERED DURING DRILLING		___ AUGER <u>3 1/4"</u> HOLLOW STEM WASHBORING FROM ___ FEET		Date: 1/30/23	Date: 2/20/23	Date: 2/20/23
		JCG DRILLER SEM LOGGER		 GEOTECHNOLOGY A Universal Engineering Sciences Company		
		Geoprobe DRILL RIG				
		HAMMER TYPE <u>Auto</u>				
REMARKS:				SR-222 From Near SR-468 To Near Campground Rd Haywood County, Tennessee		
				LOG OF BORING: SP- 1		
				Project No. J042140.01		

Drawn by: GBB	Checked by: ABM	App'vd. by: DBA
Date: 1/9/23	Date: 2/20/23	Date: 2/20/23
		
<p align="center">SR-222</p> <p align="center">From Near SR-468 To Near Campground Rd</p> <p align="center">Haywood County, Tennessee</p>		
<p align="center">LOG OF BORING: W- 4</p>		
<p align="center">Project No. J042140.01</p>		

[illegible]

NOTE: STRATIFICATION LINES REPRESENT THE APPROXIMATE BOUNDARIES BETWEEN SOIL TYPES
 LOG OF BORING 2020 JDM - ELEVATIONS J042140.01 GINT.GPJ GTINC 0638301.GPJ 2/20/23 THE TRANSITION MAY BE GRADUAL. GRAPHIC LOG FOR ILLUSTRATION PURPOSES ONLY.

Surface Elevation: <u>323.6</u> Datum <u>NAD83</u>		Completion Date: <u>12/21/22</u> Station: <u>3072+59.4</u> Offset: <u>-119.8</u>		GRAPHIC LOG	DRY UNIT WEIGHT (pcf) SPT BLOW COUNTS CORE RECOVERY/RQD	SAMPLES	SHEAR STRENGTH, tsf			
			Δ - UU/2				○ - QU/2	□ - SV		
			0.5				1.0	1.5	2.0	2.5
			STANDARD PENETRATION RESISTANCE (ASTM D 1586) ▲ N-VALUE (BLOWS PER FOOT)							
DEPTH IN FEET	ELEVATION IN FEET	DESCRIPTION OF MATERIAL	WATER CONTENT, %			PL	LL			
			10	20	30			40	50	
		Fill: 6 inches of gravel								
		Medium stiff, brown, red and gray, sandy, LEAN CLAY - CL								
5	319									
			3-3-5	SS1						
			3-3-4	SS2						
			4-4-5	SS3						
10	314	Stiff, brown to red, silty, LEAN CLAY - CL	3-5-7	SS4						
15	309	Boring terminated at 15 feet.	2-4-6	SS5						
20	304									
25	299									
30	294									

GROUNDWATER DATA

X FREE WATER NOT ENCOUNTERED DURING DRILLING

DRILLING DATA

___ AUGER 3 3/4" HOLLOW STEM WASHBORING FROM ___ FEET

KJB DRILLER JJA LOGGER

CME 750X DRILL RIG

HAMMER TYPE Auto


HAMMER EFFICIENCY 84 %

Drawn by: GBB
Date: 1/13/23

Checked by: ABM
Date: 2/20/23

App'vd. by: DBA
Date: 2/20/23

REMARKS:




SR-222
From Near SR-468 To Near Campground Rd
Haywood County, Tennessee

LOG OF BORING: W- 5

Project No. J042140.01

LOG OF BORING 2020_JDM - ELEVATIONS J042140.01 GINT.GPJ GTINC 06383031.GPJ 2/27/2020

LOG OF BORING 2020_JDM - ELEVATIONS J042140.01 GINT.GPJ GTINC 06383031.GPJ 2/27/2020

Drawn by: SEM	Checked by: ABM	App'vd. by: DBA
Date: 1/9/23	Date: 2/20/23	Date: 2/20/23
		
<p style="text-align: center;">SR-222</p> <p style="text-align: center;">From Near SR-468 To Near Campground Rd</p> <p style="text-align: center;">Haywood County, Tennessee</p>		
<p style="text-align: center;">LOG OF BORING: W- 7</p>		
<p style="text-align: center;">Project No. J042140.01</p>		

NOTE: STRATIFICATION LINES REPRESENT THE APPROXIMATE BOUNDARIES BETWEEN SOIL TYPES
 LOG OF BORING 2020 JDM - ELEVATIONS J042140.01 GINT.GPJ GTINC 0638301.GPJ 2/20/23 THE TRANSITION MAY BE GRADUAL. GRAPHIC LOG FOR ILLUSTRATION PURPOSES ONLY.

Surface Elevation: <u>308.5</u>		Completion Date: <u>12/29/22</u>		GRAPHIC LOG	DRY UNIT WEIGHT (pcf) SPT BLOW COUNTS CORE RECOVERY/RQD	SAMPLES	SHEAR STRENGTH, tsf		
Datum <u>NAD83</u>		Station: <u>3088+65.6</u>					Δ - UU/2	○ - QU/2	□ - SV
		Offset: <u>-123.1</u>					0.5	1.0	1.5
							2.0	2.5	
DEPTH IN FEET	ELEVATION IN FEET	DESCRIPTION OF MATERIAL	STANDARD PENETRATION RESISTANCE (ASTM D 1586)						
			▲ N-VALUE (BLOWS PER FOOT)						
			PLI WATER CONTENT, % LL						
			10 20 30 40 50						
5	304	Topsoil: 5 inches Soft to stiff, brown and gray, LEAN CLAY - (CL) 94% passing No. 200 sieve	2-2-2	SS1	▲	●			
			2-2-4	SS2	▲	●			
10	299		3-5-5	SS3		▲	●		
			3-3-5	SS4		▲	●		
15	294	pH = 7.8	2-2-3	SS5	▲	●			
20	289	Brown, CLAYEY SAND - (SC) 17% passing No. 200 sieve		ST6					
25	284	Soft to stiff, brown, sandy, FAT CLAY - (CH)	1-2-2	SS7	▲	●			
30	279	pH = 8.2	3-4-4	SS8	▲	●			
35	274	Very stiff to stiff, gray, FAT CLAY, little sand, trace organics - CH	5-7-9	SS9		▲	●		
40	269	pH = 8.0 resistivity = 969 ohms-cm	7-9-11	SS10		▲	●		
45	264		7-9-11	SS11		▲	●		
50	259		4-6-5	SS12		▲	●		
55	254		3-4-5	SS13		▲	●		
60	249		5-6-9	SS14		▲	●		
65	244	Stiff, gray, LEAN CLAY, little sand - (CL)	5-5-7	SS15		▲	●		
70	239	Very dense, white and brown, CLAYEY SAND - SC	17-50/3"	SS16		●			3"
75	234	Hard, white and brown, sandy, FAT CLAY - CH Boring terminated at 75 feet due to split-spoon refusal.	50/3"	SS17		●			S-3"
80	229								

GROUNDWATER DATA


ENCOUNTERED AT 23.5 FEET ∇

DRILLING DATA

___ AUGER 3 3/4" HOLLOW STEM
 WASHBORING FROM 23.5 FEET
 KJB DRILLER NMRG LOGGER
 CME 750X DRILL RIG
 HAMMER TYPE Auto
 HAMMER EFFICIENCY 84 %

Drawn by: NMRG Checked by: ABM App'vd. by: DBA
 Date: 1/3/23 Date: 2/20/23 Date: 2/20/23

REMARKS:




SR-222
 From Near SR-468 To Near Campground Rd
 Haywood County, Tennessee


LOG OF BORING: BR-1

Project No. J042140.01

NOTE: STRATIFICATION LINES REPRESENT THE APPROXIMATE BOUNDARIES BETWEEN SOIL TYPES
 LOG OF BORING 2020 JDM - ELEVATIONS J042140.01 GINT.GPJ GTINC 0638301.GPJ 2/20/23 THE TRANSITION MAY BE GRADUAL. GRAPHIC LOG FOR ILLUSTRATION PURPOSES ONLY.

Surface Elevation: <u>309.7</u>		Completion Date: <u>12/28/22</u>		GRAPHIC LOG	DRY UNIT WEIGHT (pcf) SPT BLOW COUNTS CORE RECOVERY/RQD	SAMPLES	SHEAR STRENGTH, tsf				
Datum <u>NAD83</u>		Station: <u>3089+91.6</u>					Δ - UU/2	○ - QU/2	□ - SV		
		Offset: <u>52.8</u>					0.5	1.0	1.5	2.0	2.5
							STANDARD PENETRATION RESISTANCE (ASTM D 1586)				
DEPTH IN FEET	ELEVATION IN FEET	DESCRIPTION OF MATERIAL	▲ N-VALUE (BLOWS PER FOOT)								
			WATER CONTENT, %								
				PL	10	20	30	40	50	LL	
		Topsoil: 4 inches		2-5-6	SS1						
		Stiff to medium stiff, tan to brown, sandy SILT - ML		2-2-3	SS2	▲	●				
5	305			2-3-3	SS3	▲		●			
		Medium stiff, brown to gray, clayey SILT - ML			*ST4						
10	300										
		resistivity = 2,109 ohms-cm		2-2-4	SS5	▲		●			
15	295										
		Medium stiff, brown, silty, LEAN CLAY - CL pH = 7.6		2-3-3	SS6	▲		●			
20	290										
		Soft to very stiff, brown, sandy, LEAN CLAY - (CL) restivity = 1,824 ohms-cm		2-1-3	SS7	▲		●			
25	285										
				1-1-2	SS8	▲		●			
30	280										
		61% passing No. 200 sieve pH = 6.7		4-6-6	SS9		▲	●			
35	275										
		66% passing No. 200 sieve		7-9-10	SS10		▲	●			
40	270										
		Very stiff, brown to gray, LEAN CLAY - (CL) pH = 8.1		5-7-10	SS11		▲	●			
45	265										
				5-9-12	SS12		▲	●			
50	260										
		Very stiff to stiff, brown to gray, sandy, LEAN CLAY - CL		8-12-16	SS13			●	▲		
55	255										
		pH = 7.9		7-8-10	SS14		▲	●			
60	250										
				5-7-10	SS15		▲	●			
65	245										
				5-7-9	SS16		▲	●			
70	240										
				3-4-8	SS17		▲	●			
75	235										
				3-7-11	SS18		▲	●			
80	230	Boring terminated at 80 feet.									

GROUNDWATER DATA		DRILLING DATA		Drawn by: GBB	Checked by: ABM	App'vd. by: DBA
<u>X</u> FREE WATER NOT ENCOUNTERED DURING DRILLING		<u> </u> AUGER <u>3 3/4"</u> HOLLOW STEM WASHBORING FROM <u>20</u> FEET		Date: 1/9/23	Date: 2/20/23	Date: 2/20/23
		<u>KJB</u> DRILLER <u>GBB</u> LOGGER		 GEOTECHNOLOGY A Universal Engineering Sciences Company		
		<u>CME 750X</u> DRILL RIG				
		HAMMER TYPE <u>Auto</u>				
REMARKS: <u>*No recovery</u>		HAMMER EFFICIENCY <u>84</u> %		SR-222 From Near SR-468 To Near Campground Rd Haywood County, Tennessee		
				LOG OF BORING: BR-2		
				Project No. J042140.01		


Drawn by: SEM	Checked by: ABM	App'vd. by: DBA
Date: 12/21/22	Date: 1/20/23	Date: 1/20/23
		
<p align="center">SR-222</p> <p align="center">From Near SR-468 To Near Campground Rd</p> <p align="center">Haywood County, Tennessee</p>		
<p align="center">LOG OF BORING: W- 9</p>		
<p align="center">Project No. J042140.01</p>		

LOG OF BORING 2020_JDM - ELEVATIONS J042140.01 GINT.GPJ GTINC 06383031.GPJ 2/27/2020

NOTE: STRATIFICATION LINES REPRESENT THE APPROXIMATE BOUNDARIES BETWEEN SOIL TYPES
 LOG OF BORING 2020 JDM - ELEVATIONS J042140.01 GINT.GPJ GTINC 0638301.GPJ 2/2/23 THE TRANSITION MAY BE GRADUAL. GRAPHIC LOG FOR ILLUSTRATION PURPOSES ONLY.

Surface Elevation: <u>321.8</u>		Completion Date: <u>1/4/23</u>		GRAPHIC LOG	DRY UNIT WEIGHT (pcf) SPT BLOW COUNTS CORE RECOVERY/RQD	SAMPLES	SHEAR STRENGTH, tsf				
Datum <u>NAD83</u>		Station: <u>3093+17.5</u>					Δ - UU/2	○ - QU/2	□ - SV		
		Offset: <u>-477.2</u>					0.5	1.0	1.5	2.0	2.5
							STANDARD PENETRATION RESISTANCE (ASTM D 1586) ▲ N-VALUE (BLOWS PER FOOT)				
DEPTH IN FEET	ELEVATION IN FEET	DESCRIPTION OF MATERIAL	WATER CONTENT, %			PL	LL				
			10	20	30			40	50		
		Fill: 6 inches of gravel									
		Medium stiff, brown, silty, LEAN CLAY, trace organics, gravel and sand - CL		2-3-4	SS1	▲	●				
				3-3-3	SS2	▲	●				
5	317										
		Stiff, red and brown, FAT CLAY, little sand - CH		2-5-5	SS3	▲	●				
				3-6-8	SS4	▲	●				
10	312										
		Medium stiff, orange and gray, sandy, LEAN CLAY - CL		2-4-4	SS5	▲	●				
15	307	Boring terminated at 15 feet.									
20	302										
25	297										
30	292										

GROUNDWATER DATA		DRILLING DATA	
<u>X</u> FREE WATER NOT ENCOUNTERED DURING DRILLING		___ AUGER <u>3 3/4"</u> HOLLOW STEM WASHBORING FROM ___ FEET	
		<u>KJB</u> DRILLER <u>GBB</u> LOGGER	
		<u>CME 750X</u> DRILL RIG	
		HAMMER TYPE <u>Auto</u>	
		HAMMER EFFICIENCY <u>84</u> %	
REMARKS:			


Drawn by: LLP	Checked by: ABM	App'vd. by: DBA
Date: 1/5/23	Date: 2/20/23	Date: 2/20/23
 GEOTECHNOLOGY A Universal Engineering Sciences Company		
SR-222 From Near SR-468 To Near Campground Rd Haywood County, Tennessee		
LOG OF BORING: CON-3		
Project No. J042140.01		

LOG OF BORING 2020_JDM - ELEVATIONS J042140.01 GINT.GPJ GTINC 06383031.GPJ 2/27/2020


LOG OF BORING 2020_JDM - ELEVATIONS J042140.01 GINT.GPJ GTINC 06383031.GPJ 2/27/2020


[illegible]

NOTE: STRATIFICATION LINES REPRESENT THE APPROXIMATE BOUNDARIES BETWEEN SOIL TYPES
LOG OF BORING 2020 JDM - ELEVATIONS J042140.01 GINT.GPJ GTINC 0638301.GPJ 2/20/23 THE TRANSITION MAY BE GRADUAL. GRAPHIC LOG FOR ILLUSTRATION PURPOSES ONLY.

Surface Elevation: <u>311.5</u>		Completion Date: <u>12/20/22</u>		GRAPHIC LOG	DRY UNIT WEIGHT (pcf) SPT BLOW COUNTS CORE RECOVERY/RQD	SAMPLES	SHEAR STRENGTH, tsf						
Datum <u>NAD83</u>		Station: <u>3113+18.3</u>					△ - UU/2 ○ - QU/2 □ - SV						
Offset: <u>51.8</u>							0.5 1.0 1.5 2.0 2.5						
DEPTH IN FEET	ELEVATION IN FEET	DESCRIPTION OF MATERIAL					STANDARD PENETRATION RESISTANCE (ASTM D 1586)						
							▲ N-VALUE (BLOWS PER FOOT)						
							WATER CONTENT, %						
							PL	10	20	30	40	50	LL
		Gravel: 6 inches											
		Stiff to soft, gray and brown, silty, LEAN CLAY, trace organics - CL											
					4-5-6	SS1							
					3-4-6	SS2							
5	307				5-4-5	SS3							
					2-2-2	SS4							
10	302				2-3-3	SS5							
15	297	Boring terminated at 15 feet.											
20	292												
25	287												
30	282												
GROUNDWATER DATA							DRILLING DATA						
<input checked="" type="checkbox"/> FREE WATER NOT ENCOUNTERED DURING DRILLING							<input type="checkbox"/> AUGER <u>3 3/4"</u> HOLLOW STEM WASHBORING FROM <u> </u> FEET						
REMARKS:							KJB DRILLER JWD LOGGER						
							CME 750X DRILL RIG						
							HAMMER TYPE <u>Auto</u>						
							HAMMER EFFICIENCY <u>84</u> %						
							Drawn by: SEM Checked by: ABM App'vd. by: DBA						
							Date: 1/4/23 Date: 2/20/23 Date: 2/20/23						
							 GEOTECHNOLOGY A Universal Engineering Sciences Company						
							SR-222 From Near SR-468 To Near Campground Rd Haywood County, Tennessee						
							LOG OF BORING: E-11						
							Project No. J042140.01						

[illegible]

Surface Elevation: <u>320.3</u>		Completion Date: <u>12/14/22</u>				SHEAR STRENGTH, tsf							
Datum <u>NAD83</u>		Station: <u>3118+52.3</u>				Δ - UU/2 ○ - QU/2 □ - SV 0.5 1.0 1.5 2.0 2.5							
		Offset: <u>-435.5</u>				STANDARD PENETRATION RESISTANCE (ASTM D 1586) ▲ N-VALUE (BLOWS PER FOOT)							
						WATER CONTENT, % PL ----- LL 10 20 30 40 50							
DEPTH IN FEET	ELEVATION IN FEET	DESCRIPTION OF MATERIAL		GRAPHIC LOG	DRY UNIT WEIGHT (pcf) SPT BLOW COUNTS CORE RECOVERY/RQD	SAMPLES							
		Asphalt: 10 inches											
		Medium stiff, brown and red, gravelly SILT - ML			7-4-3	SS1							
		Soft to medium stiff, brown and tan, silty, LEAN CLAY - (CL) little sand 89% passing No. 200 sieve trace organics and sand			1-2-2	SS2							
5	315				2-1-3	SS3							
					1-2-4	SS4							
10	310				2-3-4	SS5							
		Boring terminated at 15 feet.											
15	305												
20	300												
25	295												
30	290												
GROUNDWATER DATA							DRILLING DATA						
<input checked="" type="checkbox"/> FREE WATER NOT ENCOUNTERED DURING DRILLING							<input type="checkbox"/> AUGER 3 3/4" HOLLOW STEM WASHBORING FROM ___ FEET						
							KJB DRILLER JWD LOGGER						
							CME 750X DRILL RIG						
							HAMMER TYPE Auto						
							HAMMER EFFICIENCY 84 %						
REMARKS:							Drawn by: SEM Checked by: ABM App'vd. by: DBA Date: 1/9/23 Date: 2/20/23 Date: 2/20/23						
							 GEOTECHNOLOGY A Universal Engineering Sciences Company						
							SR-222 From Near SR-468 To Near Campground Rd Haywood County, Tennessee						
							LOG OF BORING: CON-5						
							Project No. J042140.01						

Drawn by: GBB	Checked by: ABM	App'vd. by: DBA
Date: 1/10/23	Date: 2/20/23	Date: 2/20/23
		
<p align="center">SR-222</p> <p align="center">From Near SR-468 To Near Campground Rd</p> <p align="center">Haywood County, Tennessee</p>		
<p align="center">LOG OF BORING: E-13</p>		
<p align="center">Project No. J042140.01</p>		

[illegible]

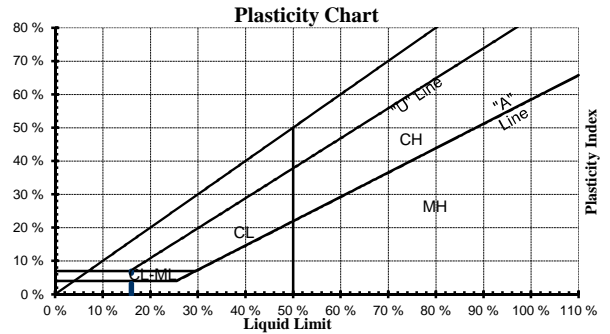
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LOG OF BORING 2020_JDM - ELEVATIONS J042140.01 GINT.GPJ GTINC 06383031.GPJ 2/27/2020

BORING LOG: TERMS AND SYMBOLS

LEGEND

CS	Continuous Sampler
GB	Grab Sample
NQ	NQ Rock Core
PST	Three-Inch Diameter Piston Tube Sample
SS	Split-Spoon Sample (Standard Penetration Test)
ST	Three-Inch Diameter Shelby Tube Sample
*	Sample Not Recovered
PL	Plastic Limit (ASTM D4318)
LL	Liquid Limit (ASTM D4318)
SV	Shear Strength from Field Vane (ASTM D2573)
UU	Shear Strength from Unconsolidated-Undrained Triaxial Compression Test (ASTM D2850)
QU	Shear Strength from Unconfined Compression Test (ASTM D2166)



SOIL GRAIN SIZE

US STANDARD SIEVE

	12"	3"	3/4"	4	10	40	200		
BOULDERS	COBBLES	GRAVEL		SAND			SILT	CLAY	
		COARSE	FINE	COARSE	MEDIUM	FINE			
		300	76.2	19.1	4.76	2.00	0.42	0.074	0.005
SOIL GRAIN SIZE IN MILLIMETERS									

UNIFIED SOIL CLASSIFICATION SYSTEM

Major Divisions			Symbol	Description
Coarse-Grained Soils (More than 50% Larger than No. 200 Sieve Size)	Gravel and Gravelly Soil	Clean Gravels Little or no Fines	GW	Well-Graded Gravel, Gravel- Sand Mixture
			GP	Poorly-Graded Gravel, Gravel-Sand Mixture
		Gravels with Appreciable Fines	GM	Silty Gravel, Gravel-Sand-Silt Mixture
			GC	Clayey-Gravel, Gravel-Sand-Clay Mixture
	Sand and Sandy Soils	Clean Sands Little or no Fines	SW	Well-Graded Sand, Gravelly Sand
			SP	Poorly-Graded Sand, Gravelly Sand
		Sands with Appreciable Fines	SM	Silty Sand, Sand-Silt Mixture
			SC	Clayey-Sand, Sand-Clay Mixture
Fine-Grained Soils (More than 50% Smaller than No. 200 Sieve Size)	Silts and Clays	Liquid Limit Less Than 50	ML	Silt, Sandy Silt, Clayey Silt, Slight Plasticity
			CL	Lean Clay, Sandy Clay, Silty Clay, Low to Medium Plasticity
			OL	Organic Silts or Lean Clays, Low Plasticity
	Silts and Clays	Liquid Limit Greater Than 50	MH	Silt, High Plasticity
			CH	Fat Clay, High Plasticity
			OH	Organic Clay, Medium to High Plasticity
	Highly Organic Soils		PT	Peat, Humus, Swamp Soil

STRENGTH OF COHESIVE SOILS

DENSITY OF GRANULAR SOILS

Consistency	Undrained Shear Strength (tsf)	Unconfined Comp. Strength (tsf)	Descriptive Term	Approximate N_{60} -Value Range
Very Soft	less than 0.125	less than 0.25	Very Loose	0 to 4
Soft	0.125 to 0.25	0.25 to 0.5	Loose	5 to 10
Medium Stiff	0.25 to 0.5	0.5 to 1.0	Medium Dense	11 to 30
Stiff	0.5 to 1.0	1.0 to 2.0	Dense	31 to 50
Very Stiff	1.0 to 2.0	2.0 to 3.0	Very Dense	>50
Hard	greater than 2.0	greater than 4.0		

N-Value (Blow Count) is the last two, 6-inch drive increments (i.e. 4/7/9, $N = 7 + 9 = 16$). Values are shown as a summation on the grid plot and shown in the Unit Dry Weight/SPT column.

RELATIVE COMPOSITION

OTHER TERMS

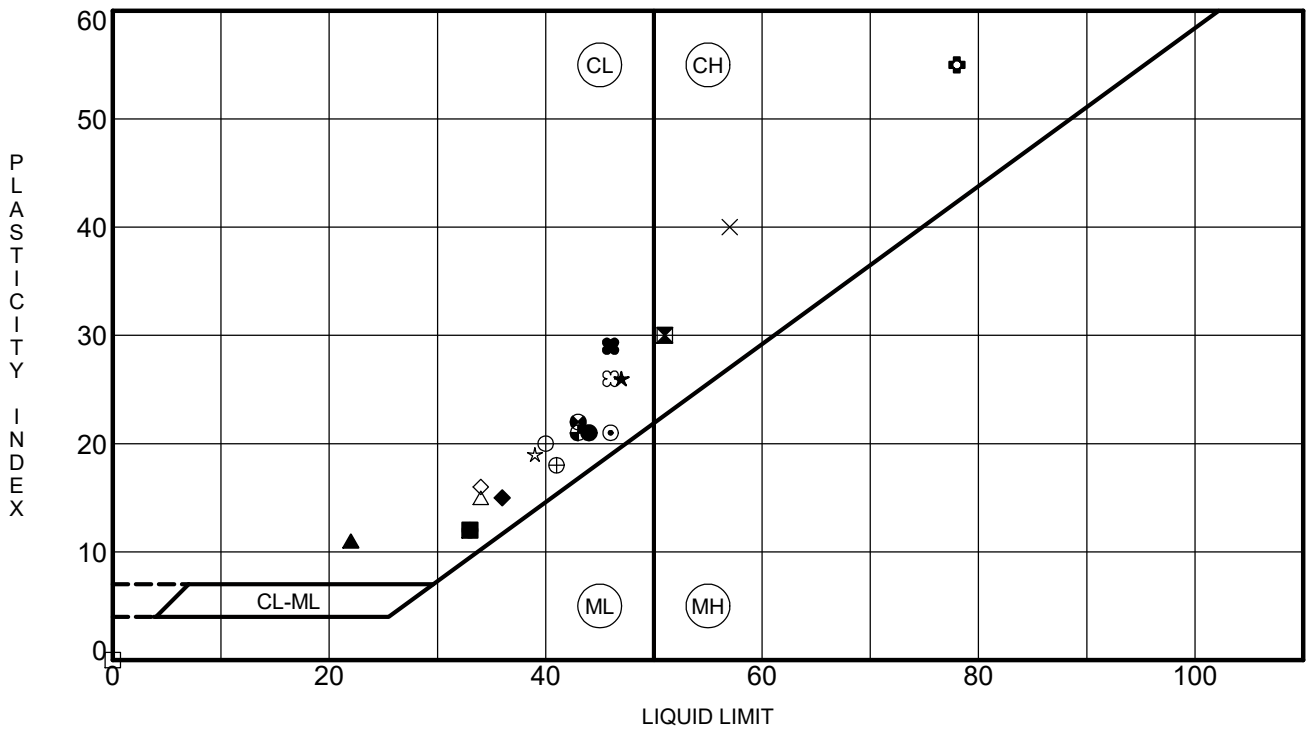
Trace	0 to 10%	Layer - Inclusion greater than 3 inches thick.
Little	10 to 20%	Seam - Inclusion 1/8-inch to 3 inches thick
Some	20 to 35%	Parting - Inclusion less than 1/8-inch thick
And	35 to 50%	Pocket - Inclusion of material that is smaller than sample diameter



Relative composition and Unified Soil Classification System (USCS) designations are based on visual descriptions and are approximate only. If laboratory tests were performed to classify the soil, the USCS designation is shown in parenthesis.



Appendix D
LABORATORY TEST DATA



	Specimen Identification		LL	PL	PI	Fines	Classification
●	BR-1	1.0	44	23	21	94	LEAN CLAY(CL), A-7-6 (22)
⊠	BR-1	23.5	51	21	30		SANDY FAT CLAY(CH), A-7-6
▲	BR-1	63.5	22	11	11		LEAN CLAY(CL), A-6
★	BR-2	33.5	47	21	26	61	SANDY LEAN CLAY(CL), A-7-6 (14)
⊙	BR-2	48.5	46	25	21		LEAN CLAY(CL), A-7-6
⊕	CON-4	8.0	78	23	55		FAT CLAY(CH), A-7-6
○	CON-5	3.5	40	20	20	89	LEAN CLAY(CL), A-6 (18)
△	CON-7	6.0	34	19	15	93	LEAN CLAY(CL), A-6 (14)
⊗	E- 1	1.0	33	21	12	95	LEAN CLAY(CL), A-6 (12)
⊕	E- 1	8.0	41	23	18		LEAN CLAY(CL), A-7-6
□	E- 3	6.0	NP	NP	NP	35	SANDY SILT(ML), A-4
⊕	E- 5	8.0	43	21	22		LEAN CLAY(CL), A-7-6
⊕	E- 7	1.0	43	22	21	95	LEAN CLAY(CL), A-7-6 (22)
☆	E- 8	3.0	39	20	19		LEAN CLAY(CL), A-6
⊗	E-12	8.0	46	20	26		LEAN CLAY(CL), A-7-6
■	E-14	1.0	33	21	12	68	SANDY LEAN CLAY(CL), A-6 (7)
◆	E-15	3.5	36	21	15	88	LEAN CLAY(CL), A-6 (13)
◇	E-16	6.0	34	18	16		LEAN CLAY(CL), A-6
×	SP- 1	3.0	57	17	40		SANDY FAT CLAY(CH), A-7-6
⬛	SP- 1	8.5	46	17	29	22	CLAYEY SAND(SC), A-2-7 (1)

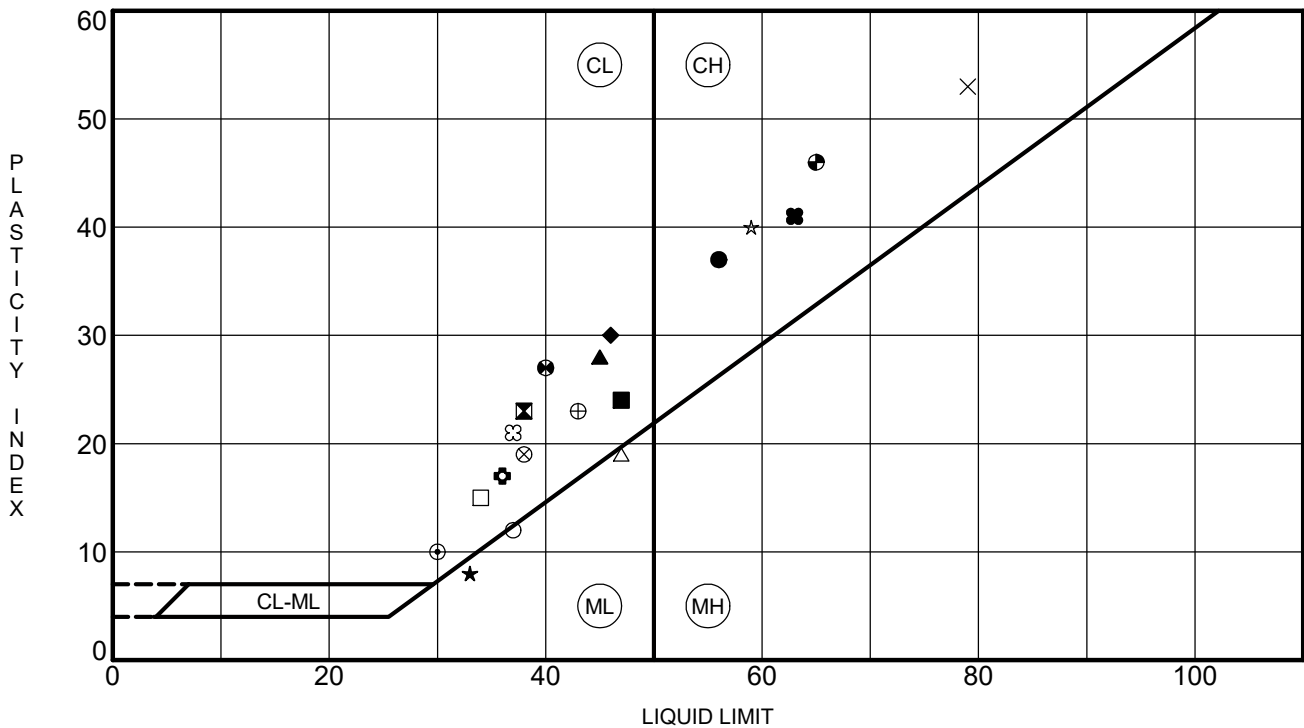


ATTERBERG LIMITS RESULTS

SR-222

From Near SR-468 To Near Campground Rd
Haywood County, Tennessee

J042140.01



	Specimen Identification		LL	PL	PI	Fines	Classification
●	SP- 2	6.0	56	19	37	77	FAT CLAY with SAND(CH), A-7-6 (29)
⊠	SP- 3	1.0	38	15	23	58	SANDY LEAN CLAY(CL), A-6 (10)
▲	SP- 3	8.0	45	17	28		SANDY LEAN CLAY(CL), A-7-6
★	SP- 4	3.0	33	25	8		SILT(ML), A-4
⊙	SP- 5	6.0	30	20	10		LEAN CLAY(CL), A-4
⊕	SP- 6	1.0	36	19	17	91	LEAN CLAY(CL), A-6 (15)
○	SP- 6	3.0	37	25	12		SILT(ML), A-6
△	SP- 7	3.0	47	28	19		SILT(ML), A-6
⊗	SP- 8	6.0	38	19	19		LEAN CLAY(CL), A-6
⊕	SP- 9	3.0	43	20	23		LEAN CLAY(CL), A-7-6
□	SP- 9	18.5	34	19	15	55	SANDY LEAN CLAY(CL), A-6 (5)
⊕	SP-10	1.0	40	13	27	93	LEAN CLAY(CL), A-6 (25)
⊕	SP-10	3.0	65	19	46		FAT CLAY(CH), A-7-6
☆	W- 1A	8.0	59	19	40		FAT CLAY(CH), A-7-6
⊗	W- 1A	23.5	37	16	21	69	SANDY LEAN CLAY(CL), A-6 (12)
■	W- 1B	3.0	47	23	24	97	LEAN CLAY(CL), A-7-6 (26)
◆	W- 2	18.0	46	16	30		LEAN CLAY(CL), A-7-6
◇	W- 3A	18.5	36	19	17	81	LEAN CLAY with SAND(CL), A-6 (13)
×	W- 3A	23.0	79	26	53	52	SANDY FAT CLAY(CH), A-7-6 (23)
⊗	W- 3B	6.0	63	22	41	60	SANDY FAT CLAY(CH), A-7-6 (22)



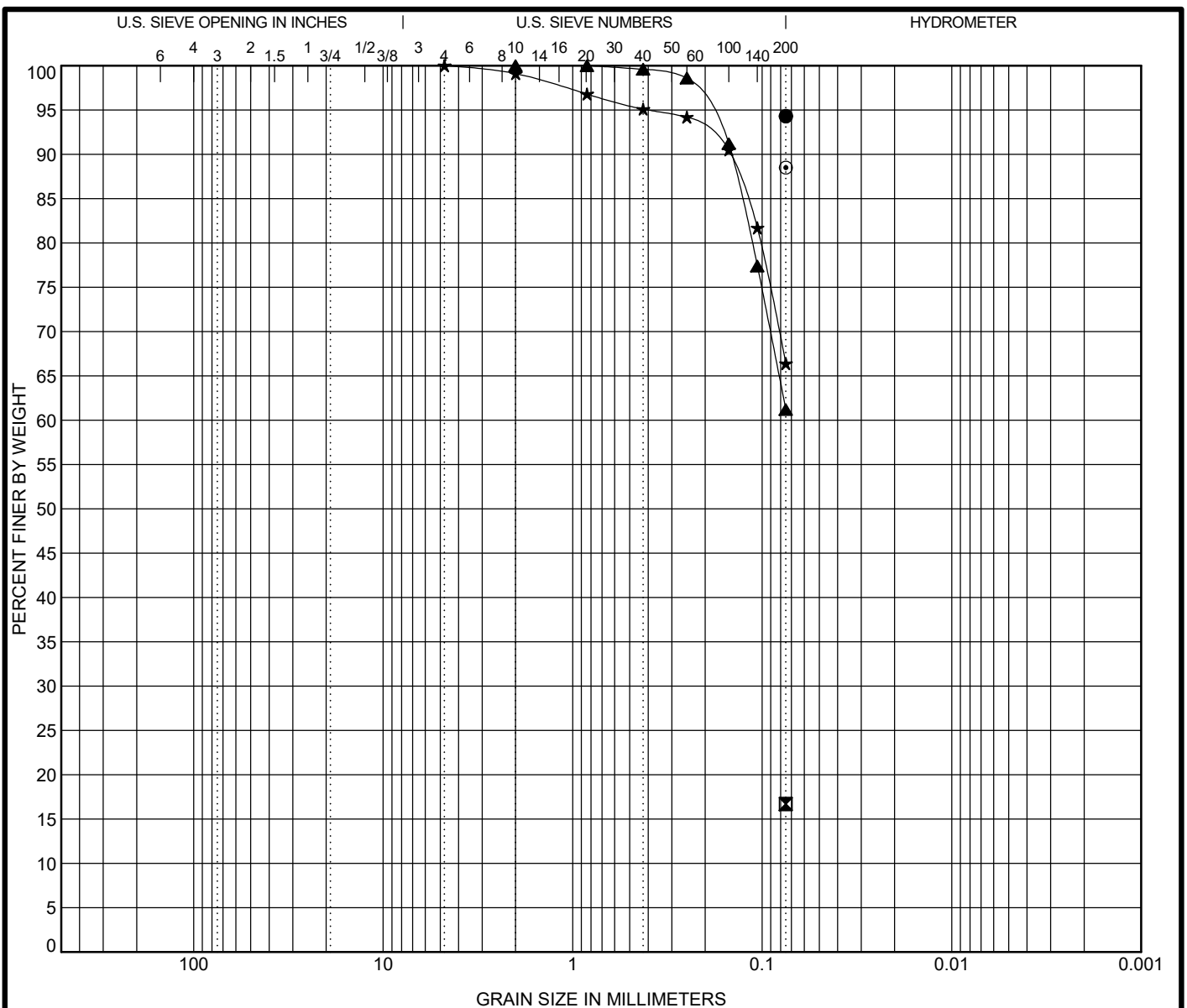
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ATTERBERG LIMITS RESULTS

SR-222

From Near SR-468 To Near Campground Rd
Haywood County, Tennessee

J042140.01



COBBLES	GRAVEL		SAND			SILT OR CLAY
	coarse	fine	coarse	medium	fine	

Specimen Identification			Classification			LL	PL	PI	Cc	Cu
●	BR-1	1.0	LEAN CLAY(CL), A-7-6 (22)			44	23	21		
☒	BR-1	18.0	CLAYEY SAND(SC), A-2-6							
▲	BR-2	33.5	SANDY LEAN CLAY(CL), A-7-6 (14)			47	21	26		
★	BR-2	38.5	SANDY LEAN CLAY(CL), A-7-6							
◎	CON-5	3.5	LEAN CLAY(CL), A-6 (18)			40	20	20		
Specimen Identification			D100	D60	D30	D10	%Gravel	%Sand	%Silt	%Clay
●	BR-1	1.0	0.075				0.0	0.0	94.3	
☒	BR-1	18.0	0.075				0.0	0.0	16.7	
▲	BR-2	33.5	2				0.0	38.8	61.2	
★	BR-2	38.5	4.75				0.0	33.6	66.4	
◎	CON-5	3.5	0.075				0.0	0.0	88.5	



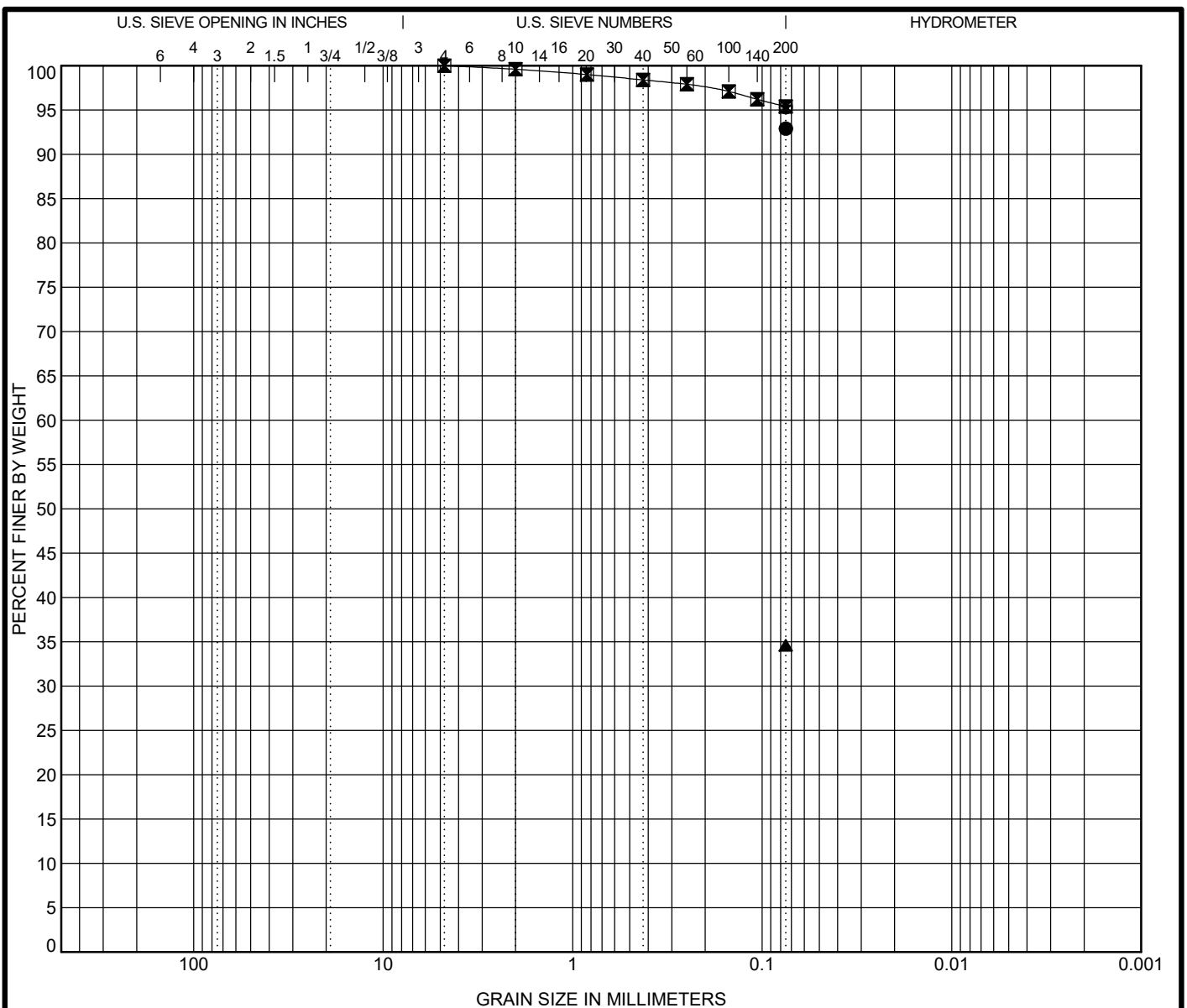
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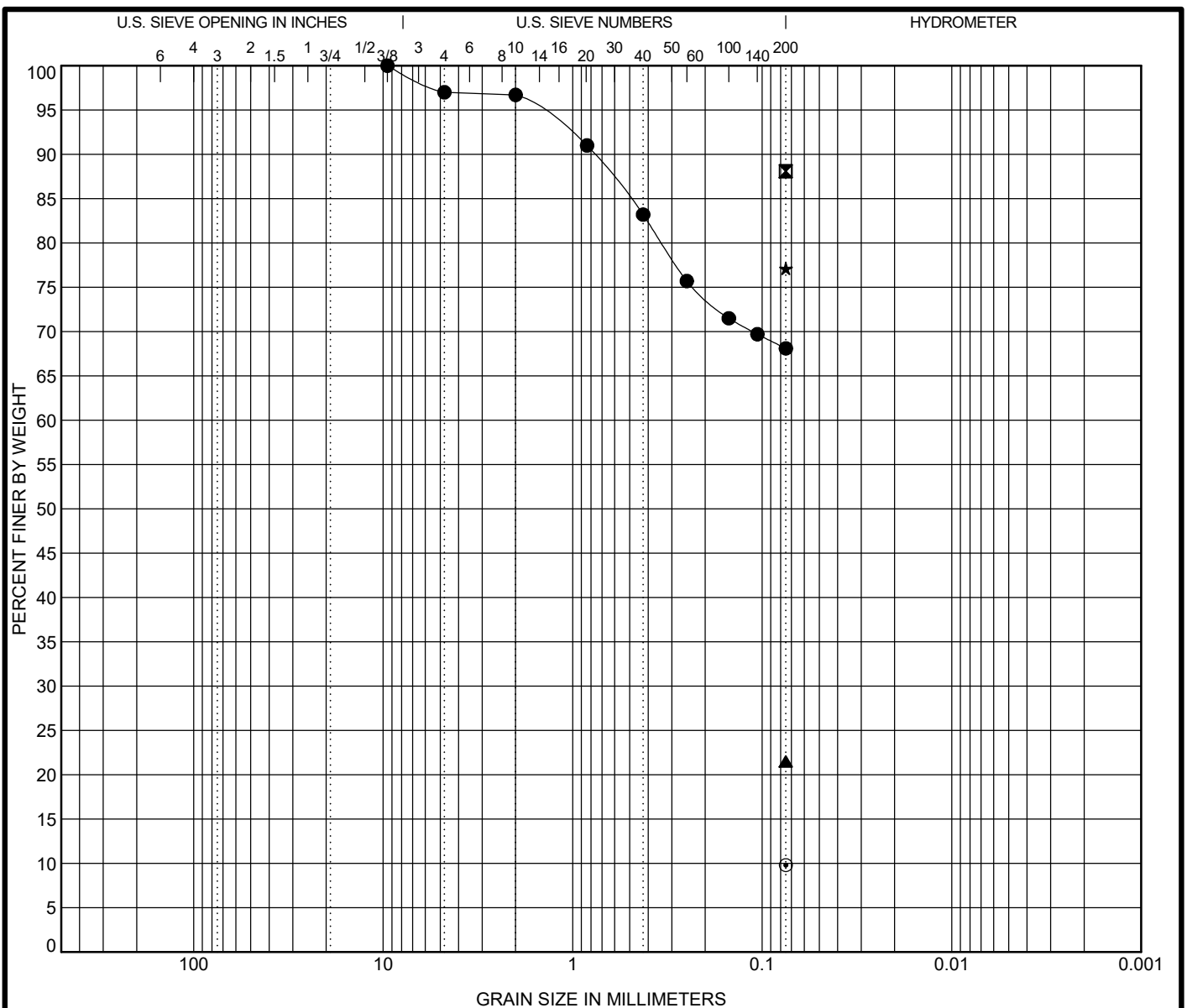
GRAIN SIZE DISTRIBUTION

SR-222

From Near SR-468 To Near Campground Rd
Haywood County, Tennessee

J042140.01





COBBLES	GRAVEL		SAND			SILT OR CLAY
	coarse	fine	coarse	medium	fine	

Specimen Identification			Classification			LL	PL	PI	Cc	Cu
●	E-14	1.0	SANDY LEAN CLAY(CL), A-6 (7)			33	21	12		
☒	E-15	3.5	LEAN CLAY(CL), A-6 (13)			36	21	15		
▲	SP- 1	8.5	CLAYEY SAND(SC), A-2-7 (1)			46	17	29		
★	SP- 2	6.0	FAT CLAY with SAND(CH), A-7-6 (29)			56	19	37		
◎	SP- 2	7.0	POORLY GRADED SAND with CLAY(SP-SC), A-2-7							
Specimen Identification			D100	D60	D30	D10	%Gravel	%Sand	%Silt	%Clay
●	E-14	1.0	9.5				3.0	28.9	68.1	
☒	E-15	3.5	0.075				0.0	0.0	88.1	
▲	SP- 1	8.5	0.075				0.0	0.0	21.5	
★	SP- 2	6.0	0.075				0.0	0.0	77.1	
◎	SP- 2	7.0	0.075				0.0	0.0	9.8	



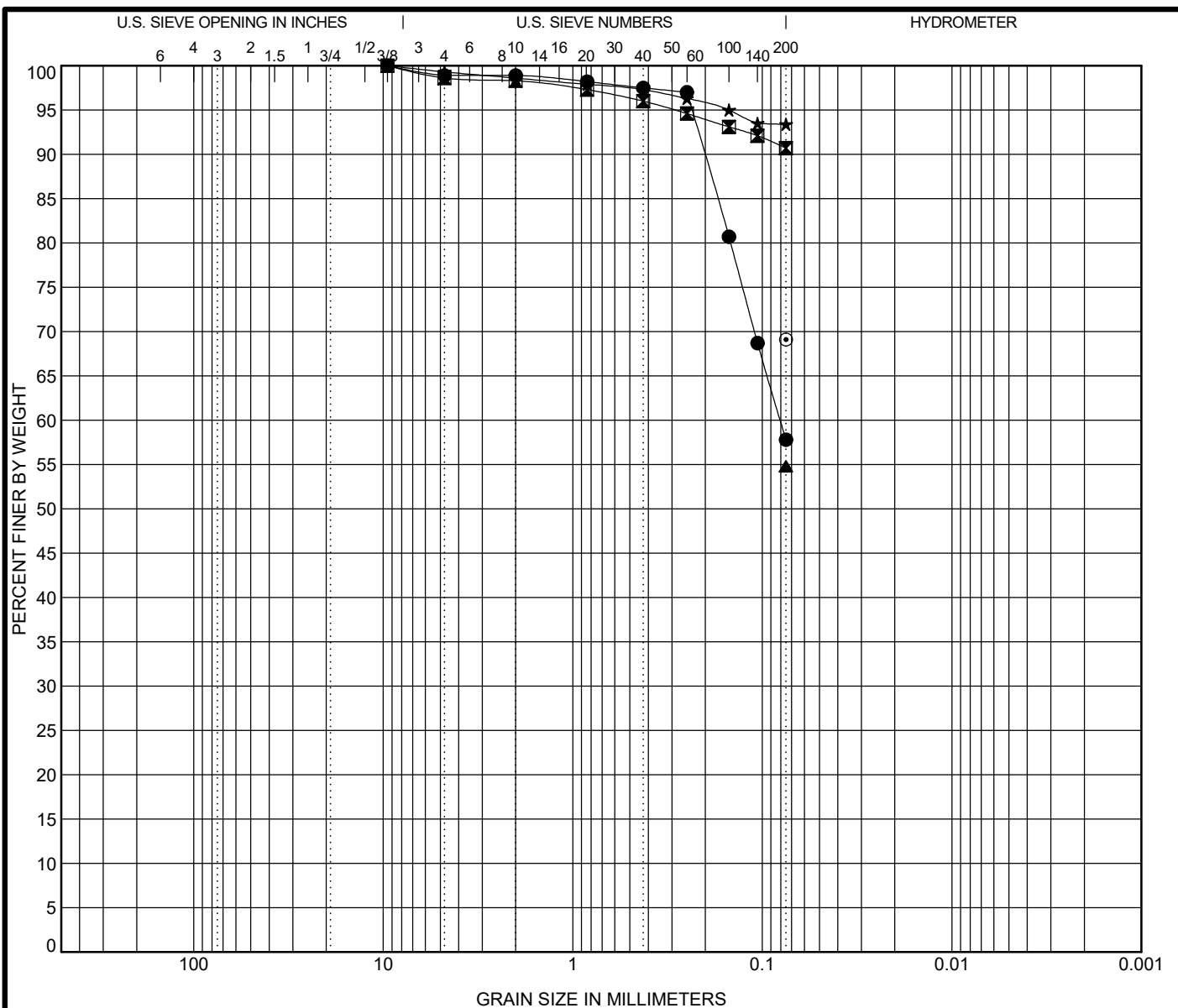
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GRAIN SIZE DISTRIBUTION

SR-222

From Near SR-468 To Near Campground Rd
Haywood County, Tennessee

J042140.01



COBBLES	GRAVEL		SAND			SILT OR CLAY
	coarse	fine	coarse	medium	fine	

Specimen Identification			Classification			LL	PL	PI	Cc	Cu
●	SP- 3	1.0	SANDY LEAN CLAY(CL), A-6 (10)			38	15	23		
☒	SP- 6	1.0	LEAN CLAY(CL), A-6 (15)			36	19	17		
▲	SP- 9	18.5	SANDY LEAN CLAY(CL), A-6 (5)			34	19	15		
★	SP-10	1.0	LEAN CLAY(CL), A-6 (25)			40	13	27		
◎	W- 1A	23.5	SANDY LEAN CLAY(CL), A-6 (12)			37	16	21		
Specimen Identification			D100	D60	D30	D10	%Gravel	%Sand	%Silt	%Clay
●	SP- 3	1.0	9.5	0.08			1.1	41.1	57.8	
☒	SP- 6	1.0	9.5				1.4	7.9	90.7	
▲	SP- 9	18.5	0.075				0.0	0.0	54.8	
★	SP-10	1.0	9.5				0.7	5.9	93.4	
◎	W- 1A	23.5	0.075				0.0	0.0	69.1	



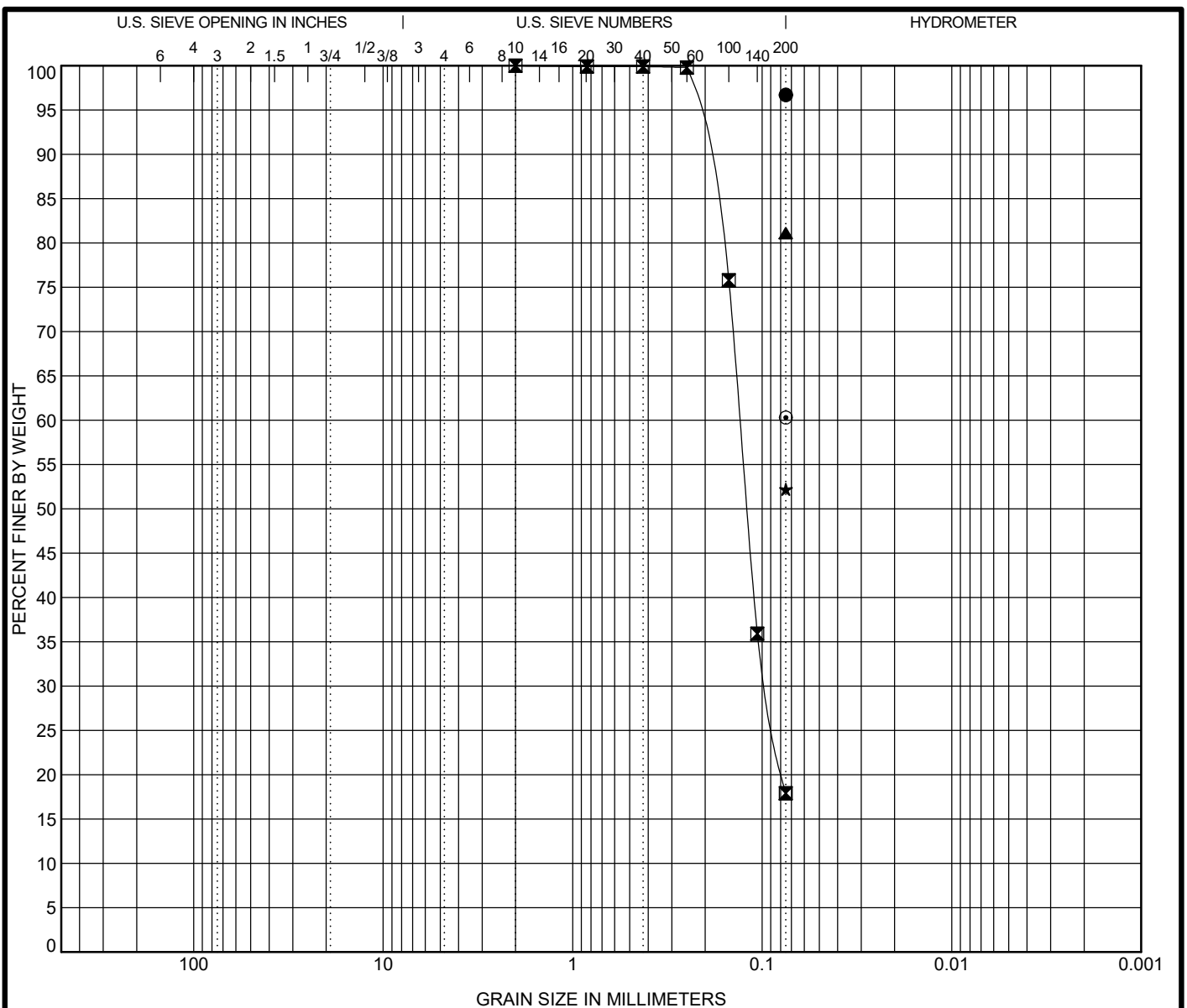
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GRAIN SIZE DISTRIBUTION

SR-222

From Near SR-468 To Near Campground Rd
Haywood County, Tennessee

J042140.01



COBBLES	GRAVEL		SAND			SILT OR CLAY
	coarse	fine	coarse	medium	fine	

Specimen Identification			Classification			LL	PL	PI	Cc	Cu
●	W- 1B	3.0	LEAN CLAY(CL), A-7-6 (26)			47	23	24		
☒	W- 3A	8.5	SILTY SAND(SM), A-2-4 (0)							
▲	W- 3A	18.5	LEAN CLAY with SAND(CL), A-6 (13)			36	19	17		
★	W- 3A	23.0	SANDY FAT CLAY(CH), A-7-6 (23)			79	26	53		
◎	W- 3B	6.0	SANDY FAT CLAY(CH), A-7-6 (22)			63	22	41		
Specimen Identification			D100	D60	D30	D10	%Gravel	%Sand	%Silt	%Clay
●	W- 1B	3.0	0.075				0.0	0.0	96.7	
☒	W- 3A	8.5	2	0.131	0.095		0.0	82.1	17.9	
▲	W- 3A	18.5	0.075				0.0	0.0	81.1	
★	W- 3A	23.0	0.075				0.0	0.0	52.2	
◎	W- 3B	6.0	0.075				0.0	0.0	60.3	



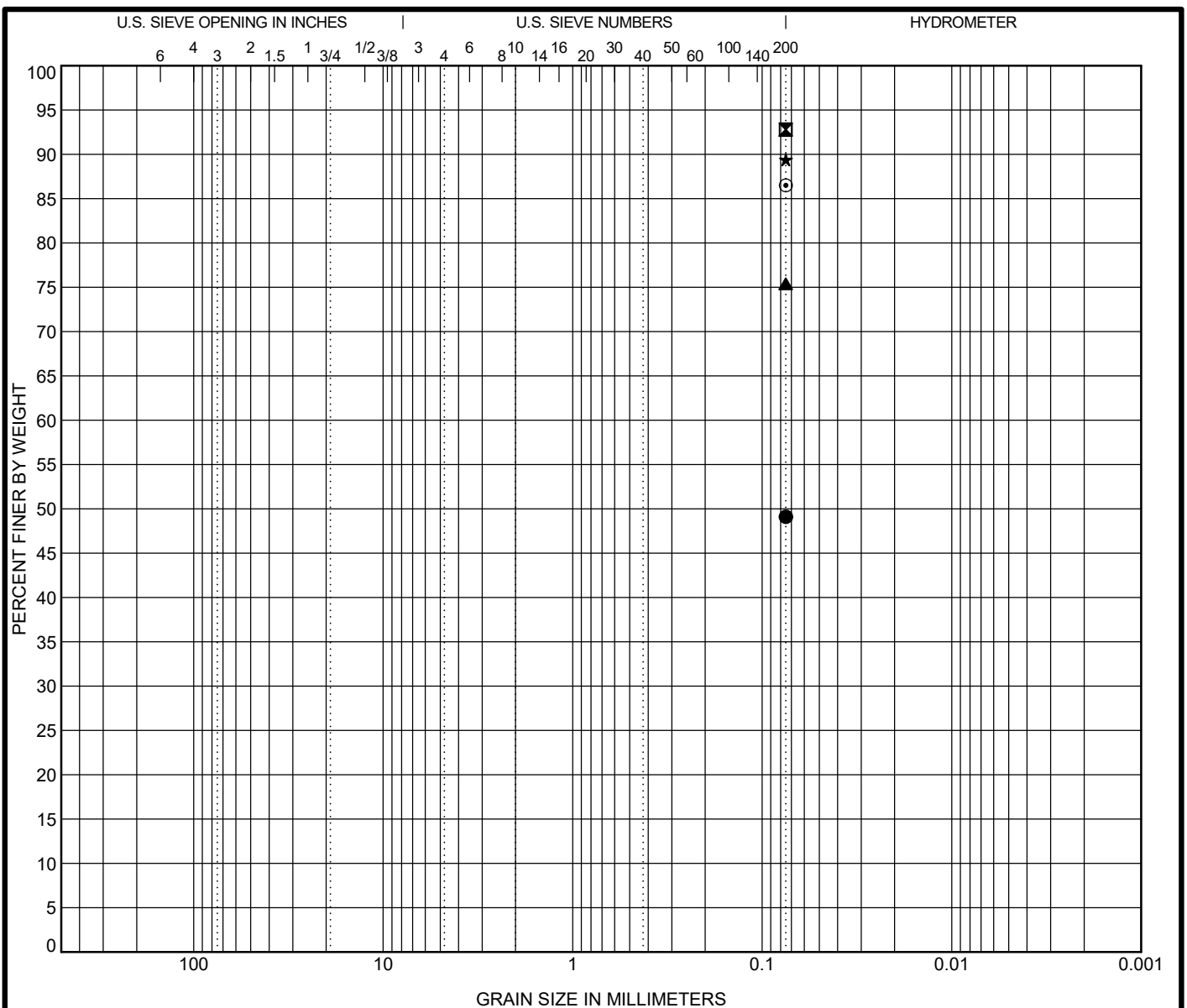
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GRAIN SIZE DISTRIBUTION

SR-222

From Near SR-468 To Near Campground Rd
Haywood County, Tennessee

J042140.01



COBBLES	GRAVEL		SAND			SILT OR CLAY
	coarse	fine	coarse	medium	fine	

Specimen Identification			Classification			LL	PL	PI	Cc	Cu
●	W-4	8.0	CLAYEY SAND(SC), A-6 (8)			38	13	25		
☒	W-9	3.5	SILT(ML), A-6							
▲	W-15	6.0	LEAN CLAY with SAND(CL), A-6 (11)			35	19	16		
★	W-18	1.0	LEAN CLAY(CL), A-6 (17)			40	22	18		
◎	W-20	3.5	LEAN CLAY(CL), A-6 (14)			34	17	17		
Specimen Identification			D100	D60	D30	D10	%Gravel	%Sand	%Silt	%Clay
●	W-4	8.0	0.075				0.0	0.0	49.1	
☒	W-9	3.5	0.075				0.0	0.0	92.8	
▲	W-15	6.0	0.075				0.0	0.0	75.4	
★	W-18	1.0	0.075				0.0	0.0	89.4	
◎	W-20	3.5	0.075				0.0	0.0	86.5	



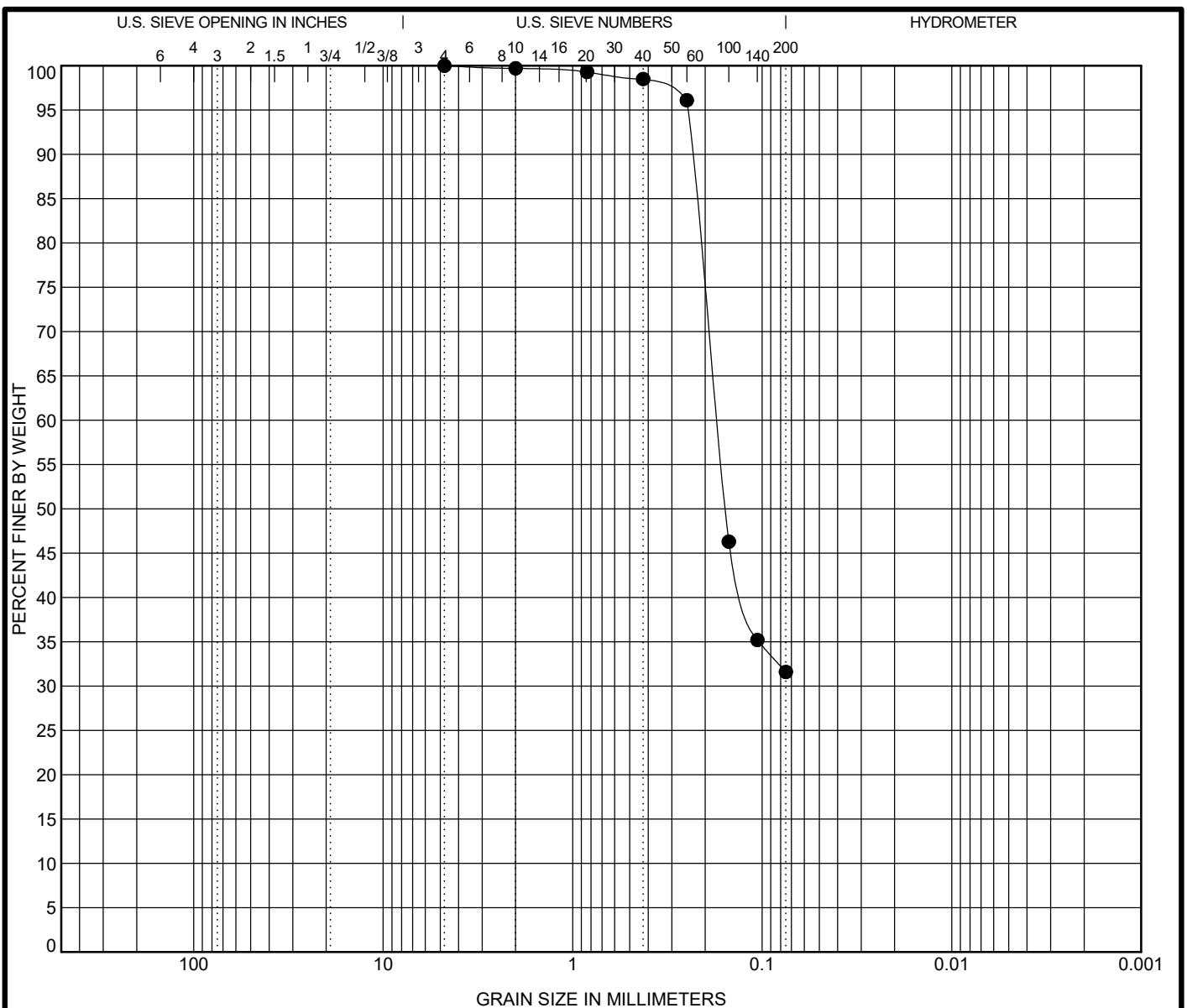
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GRAIN SIZE DISTRIBUTION

SR-222

From Near SR-468 To Near Campground Rd
Haywood County, Tennessee

J042140.01



COBBLES	GRAVEL		SAND			SILT OR CLAY
	coarse	fine	coarse	medium	fine	

Specimen Identification			Classification			LL	PL	PI	Cc	Cu
●	W-21	3.5	CLAYEY SAND(SC), A-2-6							

Specimen Identification			D100	D60	D30	D10	%Gravel	%Sand	%Silt	%Clay
●	W-21	3.5	4.75	0.173			0.0	68.4	31.6	



GRAIN SIZE DISTRIBUTION
SR-222
From Near SR-468 To Near Campground Rd
Haywood County, Tennessee
J042140.01

UNCONSOLIDATED-UNDRAINED TRIAXIAL COMPRESSION TEST ON COHESIVE SOILS ASTM D2850

CLIENT : Fisher Arnold
 PROJECT NO.: J042140.01
 PROJECT: SR-222 Widening
 LOCATION: Haywood County, Tennessee

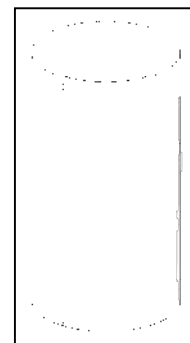
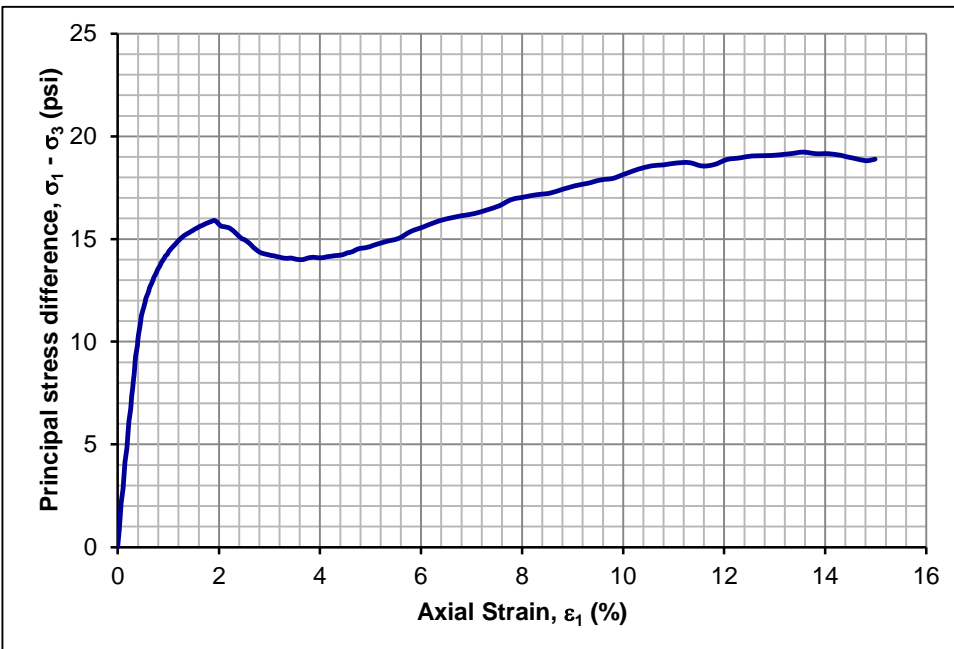
DATE: 1/26/2023

BORING NO.: CON-4	SAMPLE NO.: ST-4	DEPTH (ft.): 8.0-10.0
SAMPLE OBTAINED BY: Shelby Tube	CONDITION: Undisturbed	
SAMPLE DESCRIPTION: Stiff, red and gray, FAT CLAY - (CH)		

LIQUID LIMIT (%): 78 PLASTIC LIMIT (%): 23 PLASTICITY INDEX (%): 55 USCS: CH

SPECIFIC GRAVITY OF SOLIDS: 2.75 (Assumed) LOAD CELL NO.:

INITIAL SAMPLE DATA	FAILURE DATA***
AVERAGE DIAMETER (in.): 2.87	MOISTURE CONTENT AFTER FAILURE (%)**: 25.4
HEIGHT (in.): 6.07	AVERAGE RATE OF AXIAL STRAIN TO FAILURE (%/min.): 1.0
HEIGHT TO DIAMETER RATIO: 2.11	AXIAL STRAIN AT FAILURE (%): 13.6
WET UNIT WEIGHT (pcf): 129.5	PRINCIPAL STRESS DIFFERENCE AT FAILURE, $\sigma_1 - \sigma_3$ (psi): 19.2
DRY UNIT WEIGHT (pcf): 106.6	MINOR PRINCIPAL STRESS AT FAILURE, σ_3 (psi): 5.3
VOID RATIO: 0.61	MAJOR PRINCIPAL STRESS AT FAILURE, σ_1 (psi): 24.5
MOISTURE CONTENT (%)*: 21.5	UNDRAINED COMPRESSIVE STRENGTH, U_u (psf): 2,770
DEGREE OF SATURATION (%): 96.9	UNDRAINED SHEAR STRENGTH, s_u (psf): 1,385
	LIMITING UNDRAINED COMP. STRESS @ 10% STRAIN (psf): 2,610



REMARKS :

* Initial moisture content determined from sample cuttings.
 ** Final moisture content determined from entire sample.
 *** Failure stress values have been corrected for membrane effects.

UNCONSOLIDATED-UNDRAINED TRIAXIAL COMPRESSION TEST ON COHESIVE SOILS ASTM D2850

CLIENT : Fisher Arnold
 PROJECT NO.: J042140.01
 PROJECT: SR-222 Widening
 LOCATION: Haywood County, Tennessee

DATE: 1/19/2023

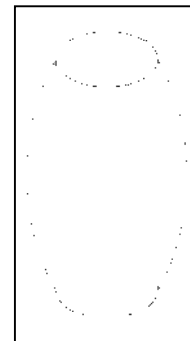
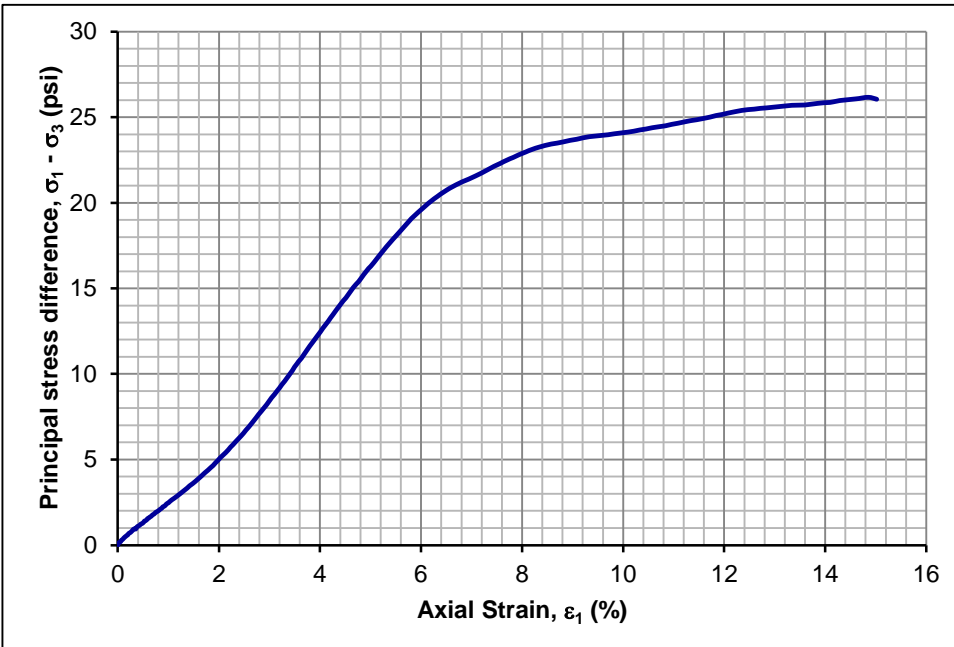
BORING NO.: E-1	SAMPLE NO.: ST-4	DEPTH (ft.): 8.0-10.0
SAMPLE OBTAINED BY: Shelby Tube	CONDITION: Undisturbed	
SAMPLE DESCRIPTION: Stiff, brown, LEAN CLAY - (CL)		

LIQUID LIMIT (%): 41 PLASTIC LIMIT (%): 23 PLASTICITY INDEX (%): 18 USCS: CL

SPECIFIC GRAVITY OF SOLIDS: 2.75 (Assumed)

LOAD CELL NO.:

INITIAL SAMPLE DATA		FAILURE DATA***	
AVERAGE DIAMETER (in.):	2.81	MOISTURE CONTENT AFTER FAILURE (%)**:	20.4
HEIGHT (in.):	5.86	AVERAGE RATE OF AXIAL STRAIN TO FAILURE (%/min.):	1.0
HEIGHT TO DIAMETER RATIO:	2.08	AXIAL STRAIN AT FAILURE (%):	14.8
WET UNIT WEIGHT (pcf):	130.0	PRINCIPAL STRESS DIFFERENCE AT FAILURE, $\sigma_1 - \sigma_3$ (psi):	26.2
DRY UNIT WEIGHT (pcf):	106.3	MINOR PRINCIPAL STRESS AT FAILURE, σ_3 (psi):	5.3
VOID RATIO:	0.61	MAJOR PRINCIPAL STRESS AT FAILURE, σ_1 (psi):	31.4
MOISTURE CONTENT (%)*:	22.4	UNDRAINED COMPRESSIVE STRENGTH, U_u (psf):	3,770
DEGREE OF SATURATION (%):	100.0	UNDRAINED SHEAR STRENGTH, s_u (psf):	1,885
		LIMITING UNDRAINED COMP. STRESS @ 10% STRAIN (psf):	3,470



REMARKS :

* Initial moisture content determined from sample cuttings.

** Final moisture content determined from entire sample.

*** Failure stress values have been corrected for membrane effects.

UNCONSOLIDATED-UNDRAINED TRIAXIAL COMPRESSION TEST ON COHESIVE SOILS ASTM D2850

CLIENT : Fisher Arnold
 PROJECT NO.: J042140.01
 PROJECT: SR-222 Widening
 LOCATION: Haywood County, Tennessee

DATE: 1/23/2023

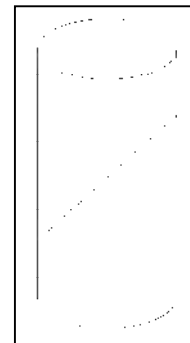
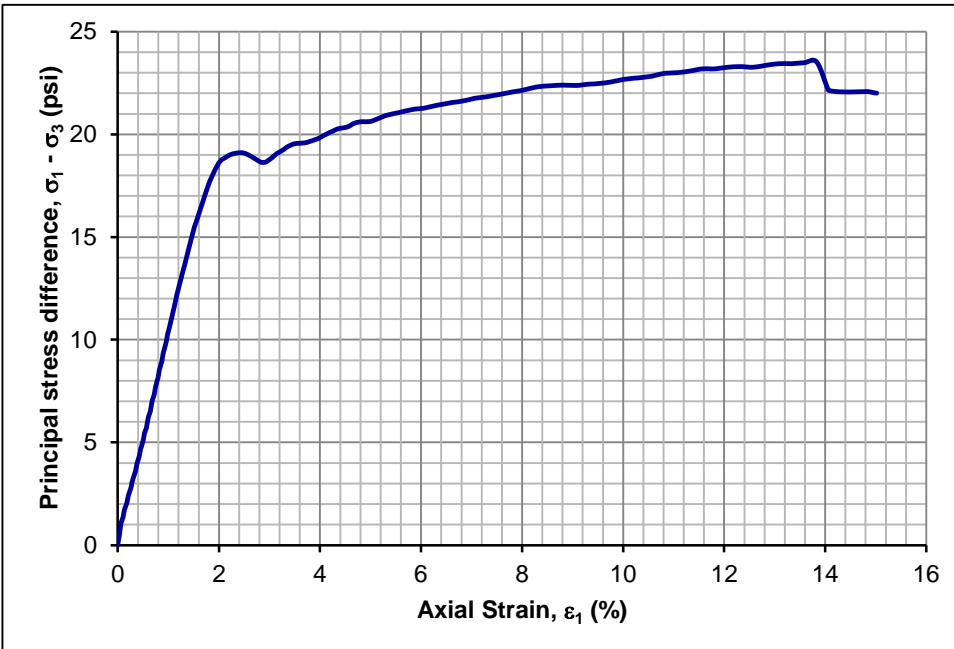
BORING NO.: E-5	SAMPLE NO.: ST-4	DEPTH (ft.): 8.0-10.0
SAMPLE OBTAINED BY: Shelby Tube	CONDITION: Undisturbed	
SAMPLE DESCRIPTION: Stiff, brown, LEAN CLAY - (CL)		

LIQUID LIMIT (%): 43 PLASTIC LIMIT (%): 21 PLASTICITY INDEX (%): 22 USCS: CL

SPECIFIC GRAVITY OF SOLIDS: 2.75 (Assumed)

LOAD CELL NO.:

INITIAL SAMPLE DATA	FAILURE DATA***
AVERAGE DIAMETER (in.): 2.84	MOISTURE CONTENT AFTER FAILURE (%)**: 25.3
HEIGHT (in.): 5.57	AVERAGE RATE OF AXIAL STRAIN TO FAILURE (%/min.): 1.0
HEIGHT TO DIAMETER RATIO: 1.96	AXIAL STRAIN AT FAILURE (%): 13.8
WET UNIT WEIGHT (pcf): 123.2	PRINCIPAL STRESS DIFFERENCE AT FAILURE, $\sigma_1 - \sigma_3$ (psi): 23.5
DRY UNIT WEIGHT (pcf): 99.0	MINOR PRINCIPAL STRESS AT FAILURE, σ_3 (psi): 5.3
VOID RATIO: 0.73	MAJOR PRINCIPAL STRESS AT FAILURE, σ_1 (psi): 28.8
MOISTURE CONTENT (%)*: 24.4	UNDRAINED COMPRESSIVE STRENGTH, U_u (psf): 3,390
DEGREE OF SATURATION (%): 91.5	UNDRAINED SHEAR STRENGTH, s_u (psf): 1,695
	LIMITING UNDRAINED COMP. STRESS @ 10% STRAIN (psf): 3,265



REMARKS :

* Initial moisture content determined from sample cuttings.
 ** Final moisture content determined from entire sample.
 *** Failure stress values have been corrected for membrane effects.

UNCONSOLIDATED-UNDRAINED TRIAXIAL COMPRESSION TEST ON COHESIVE SOILS ASTM D2850

CLIENT : Fisher Arnold
 PROJECT NO.: J042140.01
 PROJECT: SR-222 Widening
 LOCATION: Haywood County, Tennessee

DATE: 1/23/2023

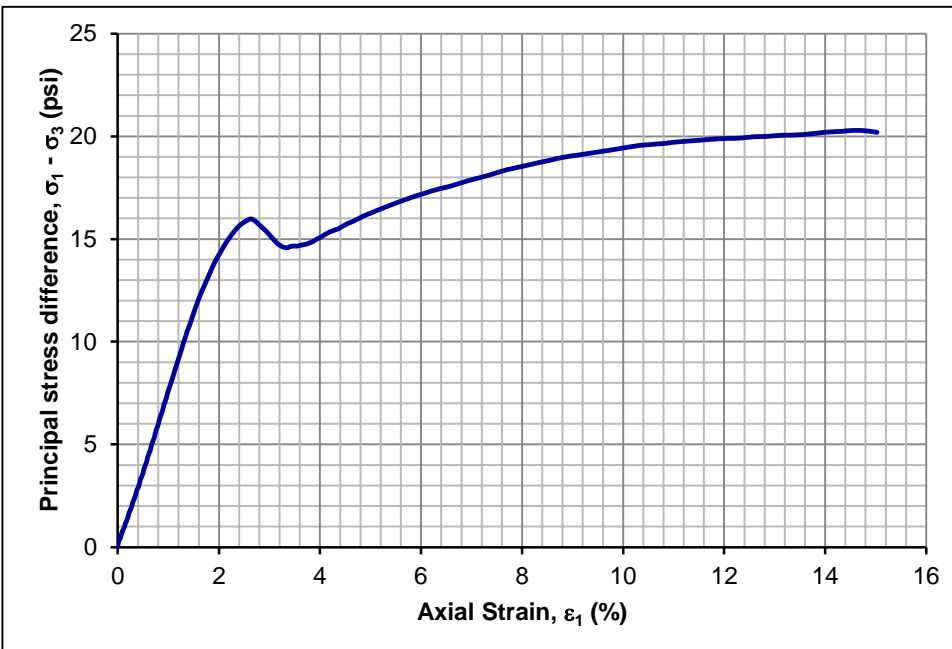
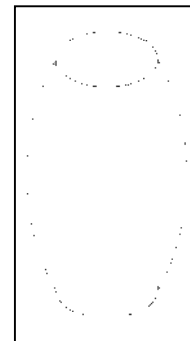
BORING NO.: E-8 SAMPLE NO.: ST-3 DEPTH (ft.): 3.0-5.0
 SAMPLE OBTAINED BY: Shelby Tube CONDITION: Undisturbed
 SAMPLE DESCRIPTION: Stiff, brown, LEAN CLAY - (CL)

LIQUID LIMIT (%): 39 PLASTIC LIMIT (%): 20 PLASTICITY INDEX (%): 19 USCS: CL

SPECIFIC GRAVITY OF SOLIDS: 2.75 (Assumed) LOAD CELL NO.:

INITIAL SAMPLE DATA		FAILURE DATA***	
AVERAGE DIAMETER (in.):	2.85	MOISTURE CONTENT AFTER FAILURE (%)**:	24.4
HEIGHT (in.):	5.58	AVERAGE RATE OF AXIAL STRAIN TO FAILURE (%/min.):	1.0
HEIGHT TO DIAMETER RATIO:	1.96	AXIAL STRAIN AT FAILURE (%):	14.6
WET UNIT WEIGHT (pcf):	124.2	PRINCIPAL STRESS DIFFERENCE AT FAILURE, $\sigma_1 - \sigma_3$ (psi):	20.3
DRY UNIT WEIGHT (pcf):	100.5	MINOR PRINCIPAL STRESS AT FAILURE, σ_3 (psi):	2.3
VOID RATIO:	0.71	MAJOR PRINCIPAL STRESS AT FAILURE, σ_1 (psi):	22.6
MOISTURE CONTENT (%)*:	23.5	UNDRAINED COMPRESSIVE STRENGTH, U_u (psf):	2,920
DEGREE OF SATURATION (%):	91.6	UNDRAINED SHEAR STRENGTH, s_u (psf):	1,460
		LIMITING UNDRAINED COMP. STRESS @ 10% STRAIN (psf):	2,800

FAILURE SHAPES



REMARKS :

* Initial moisture content determined from sample cuttings.

** Final moisture content determined from entire sample.

*** Failure stress values have been corrected for membrane effects.

UNCONSOLIDATED-UNDRAINED TRIAXIAL COMPRESSION TEST ON COHESIVE SOILS ASTM D2850

CLIENT : Fisher Arnold
 PROJECT NO.: J042140.01
 PROJECT: SR-222 Widening
 LOCATION: Haywood County, Tennessee

DATE: 1/24/2023

BORING NO.: E-12	SAMPLE NO.: ST-3	DEPTH (ft.): 8.0-10.0
SAMPLE OBTAINED BY: Shelby Tube	CONDITION: Undisturbed	
SAMPLE DESCRIPTION: Stiff, brown, LEAN CLAY - (CL)		

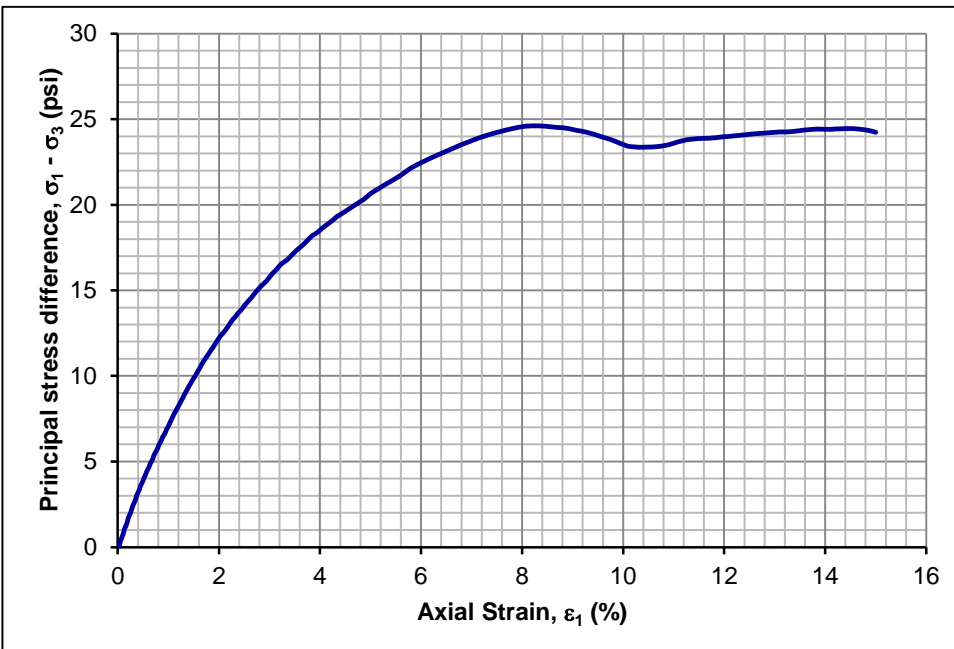
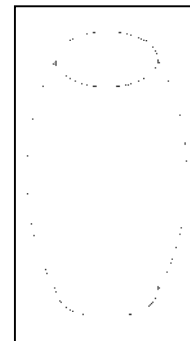
LIQUID LIMIT (%): 46 PLASTIC LIMIT (%): 20 PLASTICITY INDEX (%): 26 USCS: CL

SPECIFIC GRAVITY OF SOLIDS: 2.75 (Assumed)

LOAD CELL NO.:

INITIAL SAMPLE DATA	FAILURE DATA***
AVERAGE DIAMETER (in.): 2.85	MOISTURE CONTENT AFTER FAILURE (%)**: 24.7
HEIGHT (in.): 6.12	AVERAGE RATE OF AXIAL STRAIN TO FAILURE (%/min.): 1.0
HEIGHT TO DIAMETER RATIO: 2.15	AXIAL STRAIN AT FAILURE (%): 8.3
WET UNIT WEIGHT (pcf): 127.6	PRINCIPAL STRESS DIFFERENCE AT FAILURE, $\sigma_1 - \sigma_3$ (psi): 24.6
DRY UNIT WEIGHT (pcf): 101.9	MINOR PRINCIPAL STRESS AT FAILURE, σ_3 (psi): 5.3
VOID RATIO: 0.68	MAJOR PRINCIPAL STRESS AT FAILURE, σ_1 (psi): 29.9
MOISTURE CONTENT (%)*: 25.2	UNDRAINED COMPRESSIVE STRENGTH, U_u (psf): 3,540
DEGREE OF SATURATION (%): 100.0	UNDRAINED SHEAR STRENGTH, s_u (psf): 1,770
	LIMITING UNDRAINED COMP. STRESS @ 10% STRAIN (psf): N/A

FAILURE SHAPES



REMARKS :

* Initial moisture content determined from sample cuttings.

** Final moisture content determined from entire sample.

*** Failure stress values have been corrected for membrane effects.

UNCONSOLIDATED-UNDRAINED TRIAXIAL COMPRESSION TEST ON COHESIVE SOILS ASTM D2850

CLIENT : Fisher Arnold
 PROJECT NO.: J042140.01
 PROJECT: SR-222 Widening
 LOCATION: Haywood County, Tennessee

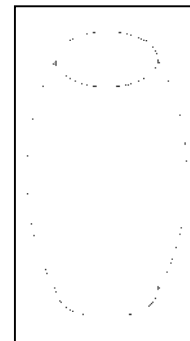
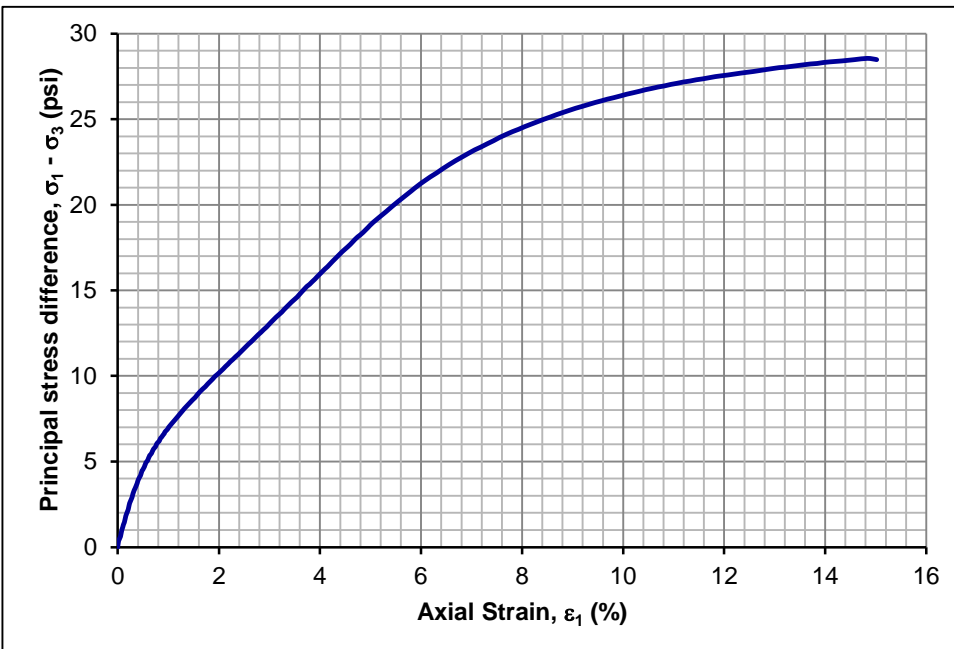
DATE: 2/2/2023

BORING NO.: SP-1 SAMPLE NO.: ST-2 DEPTH (ft.): 3.0-5.0
 SAMPLE OBTAINED BY: Shelby Tube CONDITION: Undisturbed
 SAMPLE DESCRIPTION: Very stiff, gray, sandy, FAT CLAY - (CH)

LIQUID LIMIT (%): 57 PLASTIC LIMIT (%): 17 PLASTICITY INDEX (%): 40 USCS: CH

SPECIFIC GRAVITY OF SOLIDS: 2.75 (Assumed) LOAD CELL NO.:

INITIAL SAMPLE DATA		FAILURE DATA***	
AVERAGE DIAMETER (in.):	2.83	MOISTURE CONTENT AFTER FAILURE (%)**:	20.9
HEIGHT (in.):	5.68	AVERAGE RATE OF AXIAL STRAIN TO FAILURE (%/min.):	1.0
HEIGHT TO DIAMETER RATIO:	2.01	AXIAL STRAIN AT FAILURE (%):	14.8
WET UNIT WEIGHT (pcf):	129.2	PRINCIPAL STRESS DIFFERENCE AT FAILURE, $\sigma_1 - \sigma_3$ (psi):	28.6
DRY UNIT WEIGHT (pcf):	106.5	MINOR PRINCIPAL STRESS AT FAILURE, σ_3 (psi):	2.3
VOID RATIO:	0.61	MAJOR PRINCIPAL STRESS AT FAILURE, σ_1 (psi):	30.9
MOISTURE CONTENT (%)*:	21.3	UNDRAINED COMPRESSIVE STRENGTH, U_u (psf):	4,110
DEGREE OF SATURATION (%):	96.0	UNDRAINED SHEAR STRENGTH, s_u (psf):	2,055
		LIMITING UNDRAINED COMP. STRESS @ 10% STRAIN (psf):	3,800



REMARKS :

* Initial moisture content determined from sample cuttings.
 ** Final moisture content determined from entire sample.
 *** Failure stress values have been corrected for membrane effects.

UNCONSOLIDATED-UNDRAINED TRIAXIAL COMPRESSION TEST ON COHESIVE SOILS ASTM D2850

CLIENT : Fisher Arnold
 PROJECT NO.: J042140.01
 PROJECT: SR-222 Widening
 LOCATION: Haywood County, Tennessee

DATE: 2/20/2023

BORING NO.: SP-4
 SAMPLE OBTAINED BY: Shelby Tube
 SAMPLE DESCRIPTION: Stiff, brown SILT - (ML)

SAMPLE NO.: ST-2
 CONDITION: Undisturbed

DEPTH (ft.): 3.0-5.0

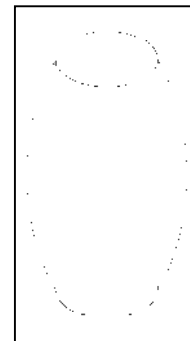
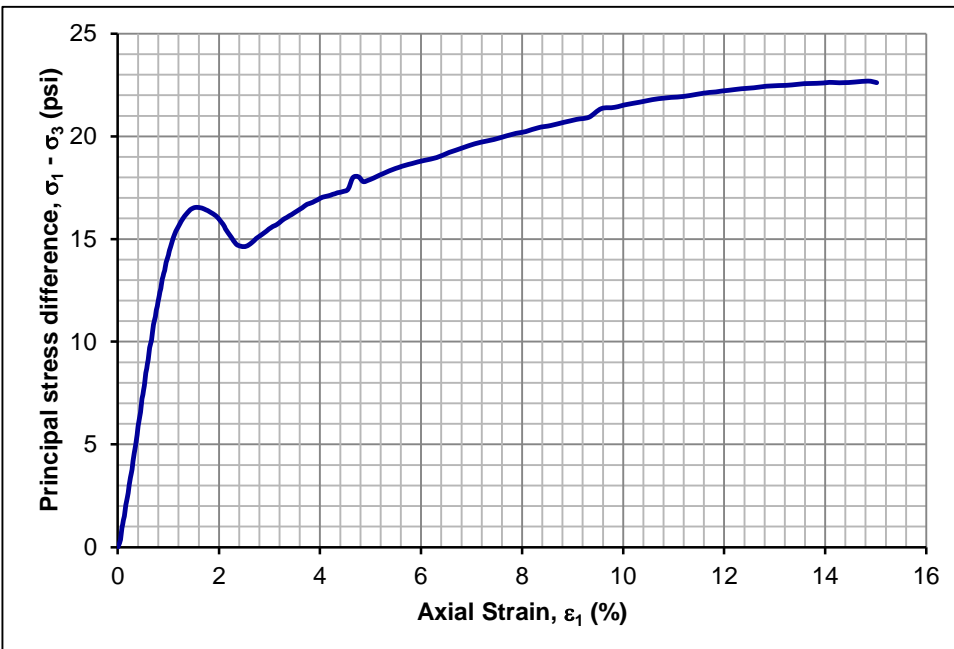
LIQUID LIMIT (%): 33 PLASTIC LIMIT (%): 25 PLASTICITY INDEX (%): 8 USCS: ML

SPECIFIC GRAVITY OF SOLIDS: 2.75 (Assumed)

LOAD CELL NO.:

INITIAL SAMPLE DATA	
AVERAGE DIAMETER (in.):	2.81
HEIGHT (in.):	5.60
HEIGHT TO DIAMETER RATIO:	1.99
WET UNIT WEIGHT (pcf):	127.8
DRY UNIT WEIGHT (pcf):	104.7
VOID RATIO:	0.64
MOISTURE CONTENT (%)*:	22.0
DEGREE OF SATURATION (%):	94.8

FAILURE DATA***	
MOISTURE CONTENT AFTER FAILURE (%)**:	36.1
AVERAGE RATE OF AXIAL STRAIN TO FAILURE (%/min.):	1.0
AXIAL STRAIN AT FAILURE (%):	14.8
PRINCIPAL STRESS DIFFERENCE AT FAILURE, $\sigma_1 - \sigma_3$ (psi):	22.7
MINOR PRINCIPAL STRESS AT FAILURE, σ_3 (psi):	2.3
MAJOR PRINCIPAL STRESS AT FAILURE, σ_1 (psi):	25.0
UNDRAINED COMPRESSIVE STRENGTH, U_u (psf):	3,270
UNDRAINED SHEAR STRENGTH, s_u (psf):	1,635
LIMITING UNDRAINED COMP. STRESS @ 10% STRAIN (psf):	3,100



REMARKS :

* Initial moisture content determined from sample cuttings.

** Final moisture content determined from entire sample.

*** Failure stress values have been corrected for membrane effects.

UNCONSOLIDATED-UNDRAINED TRIAXIAL COMPRESSION TEST ON COHESIVE SOILS ASTM D2850

CLIENT : Fisher Arnold
 PROJECT NO.: J042140.01
 PROJECT: SR-222 Widening
 LOCATION: Haywood County, Tennessee

DATE: 2/3/2023

BORING NO.: SP-6
 SAMPLE OBTAINED BY: Shelby Tube
 SAMPLE DESCRIPTION: Stiff, brown SILT - (ML)

SAMPLE NO.: ST-2
 CONDITION: Undisturbed

DEPTH (ft.): 3.0-5.0

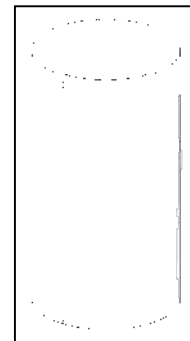
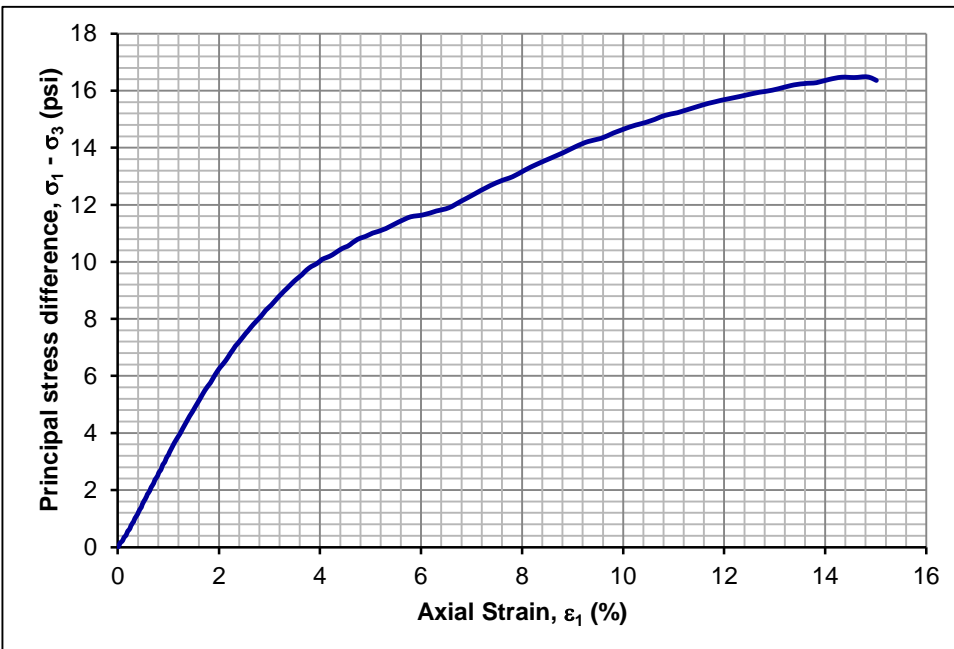
LIQUID LIMIT (%): 37 PLASTIC LIMIT (%): 25 PLASTICITY INDEX (%): 12 USCS: ML

SPECIFIC GRAVITY OF SOLIDS: 2.75 (Assumed)

LOAD CELL NO.:

INITIAL SAMPLE DATA	
AVERAGE DIAMETER (in.):	2.84
HEIGHT (in.):	6.00
HEIGHT TO DIAMETER RATIO:	2.11
WET UNIT WEIGHT (pcf):	124.9
DRY UNIT WEIGHT (pcf):	98.4
VOID RATIO:	0.74
MOISTURE CONTENT (%)*:	26.9
DEGREE OF SATURATION (%):	99.5

FAILURE DATA***	
MOISTURE CONTENT AFTER FAILURE (%)**:	26.2
AVERAGE RATE OF AXIAL STRAIN TO FAILURE (%/min.):	1.0
AXIAL STRAIN AT FAILURE (%):	14.8
PRINCIPAL STRESS DIFFERENCE AT FAILURE, $\sigma_1 - \sigma_3$ (psi):	16.5
MINOR PRINCIPAL STRESS AT FAILURE, σ_3 (psi):	2.3
MAJOR PRINCIPAL STRESS AT FAILURE, σ_1 (psi):	18.8
UNDRAINED COMPRESSIVE STRENGTH, U_u (psf):	2,370
UNDRAINED SHEAR STRENGTH, s_u (psf):	1,185
LIMITING UNDRAINED COMP. STRESS @ 10% STRAIN (psf):	2,110



REMARKS :

* Initial moisture content determined from sample cuttings.

** Final moisture content determined from entire sample.

*** Failure stress values have been corrected for membrane effects.

UNCONSOLIDATED-UNDRAINED TRIAXIAL COMPRESSION TEST ON COHESIVE SOILS ASTM D2850

CLIENT : Fisher Arnold
 PROJECT NO.: J042140.01
 PROJECT: SR-222 Widening
 LOCATION: Haywood County, Tennessee

DATE: 2/3/2023

BORING NO.: SP-7
 SAMPLE OBTAINED BY: Shelby Tube
 SAMPLE DESCRIPTION: Stiff, brown SILT - (ML)

SAMPLE NO.: ST-2
 CONDITION: Undisturbed

DEPTH (ft.): 3.0-5.0

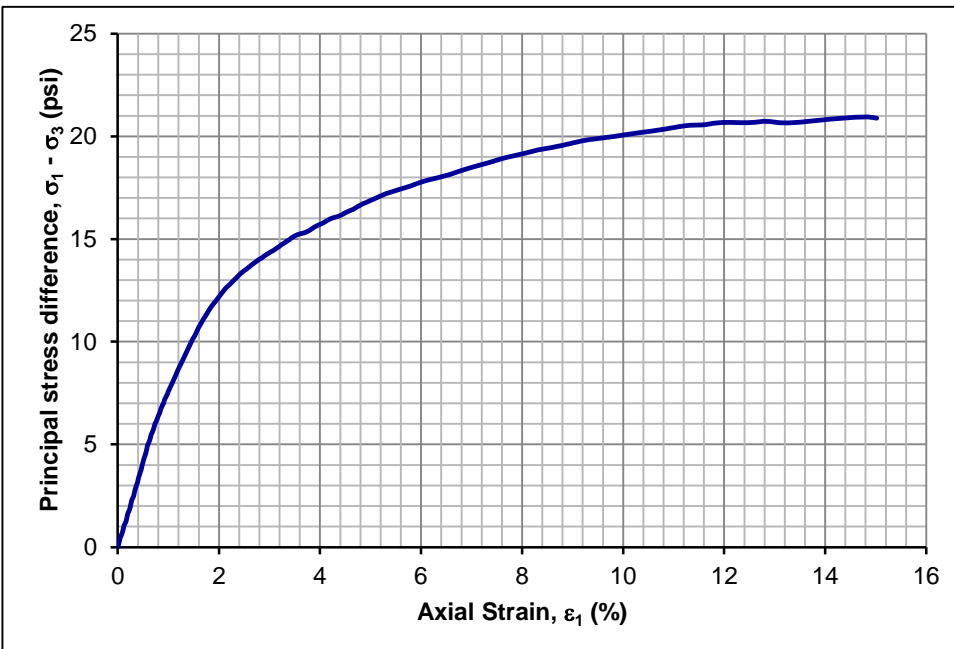
LIQUID LIMIT (%): 47 PLASTIC LIMIT (%): 28 PLASTICITY INDEX (%): 19 USCS: ML

SPECIFIC GRAVITY OF SOLIDS: 2.75 (Assumed)

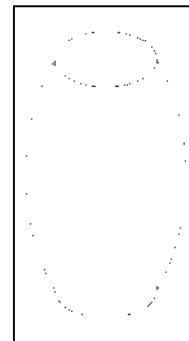
LOAD CELL NO.:

INITIAL SAMPLE DATA	
AVERAGE DIAMETER (in.):	2.83
HEIGHT (in.):	6.17
HEIGHT TO DIAMETER RATIO:	2.18
WET UNIT WEIGHT (pcf):	123.2
DRY UNIT WEIGHT (pcf):	98.1
VOID RATIO:	0.75
MOISTURE CONTENT (%)*:	25.6
DEGREE OF SATURATION (%):	94.0

FAILURE DATA***	
MOISTURE CONTENT AFTER FAILURE (%)**:	25.8
AVERAGE RATE OF AXIAL STRAIN TO FAILURE (%/min.):	1.0
AXIAL STRAIN AT FAILURE (%):	14.8
PRINCIPAL STRESS DIFFERENCE AT FAILURE, $\sigma_1 - \sigma_3$ (psi):	20.9
MINOR PRINCIPAL STRESS AT FAILURE, σ_3 (psi):	2.3
MAJOR PRINCIPAL STRESS AT FAILURE, σ_1 (psi):	23.3
UNDRAINED COMPRESSIVE STRENGTH, U_u (psf):	3,020
UNDRAINED SHEAR STRENGTH, s_u (psf):	1,510
LIMITING UNDRAINED COMP. STRESS @ 10% STRAIN (psf):	2,890



FAILURE SHAPES



REMARKS :

* Initial moisture content determined from sample cuttings.

** Final moisture content determined from entire sample.

*** Failure stress values have been corrected for membrane effects.

UNCONSOLIDATED-UNDRAINED TRIAXIAL COMPRESSION TEST ON COHESIVE SOILS ASTM D2850

CLIENT : Fisher Arnold
 PROJECT NO.: J042140.01
 PROJECT: SR-222 Widening
 LOCATION: Haywood County, Tennessee

DATE: 2/3/2023

BORING NO.: SP-8	SAMPLE NO.: ST-3	DEPTH (ft.): 6.0-8.0
SAMPLE OBTAINED BY: Shelby Tube	CONDITION: Undisturbed	
SAMPLE DESCRIPTION: Very stiff, tan, LEAN CLAY - (CL)		

LIQUID LIMIT (%): 38 PLASTIC LIMIT (%): 19 PLASTICITY INDEX (%): 19 USCS: CL

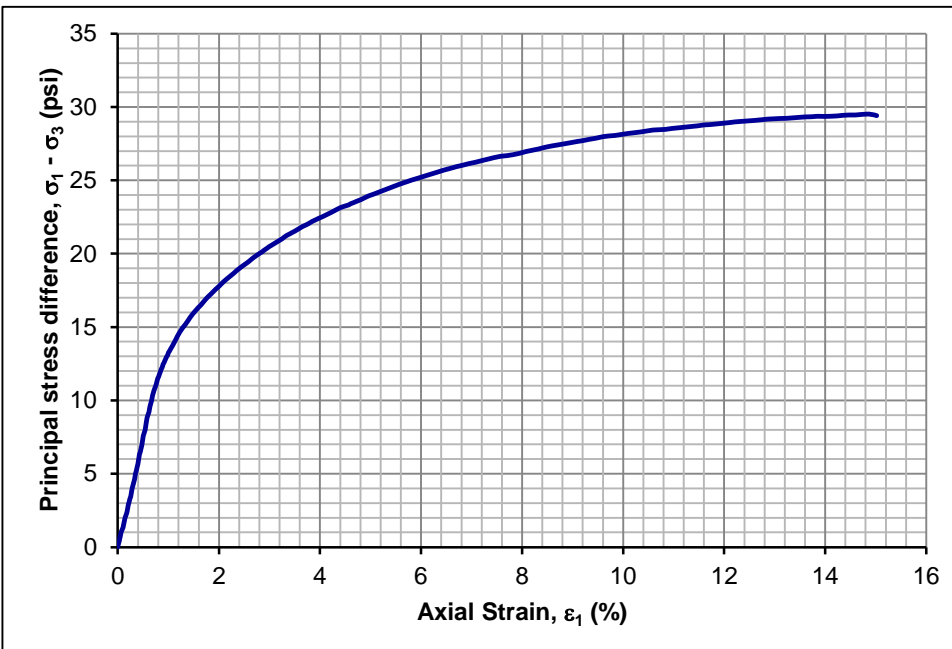
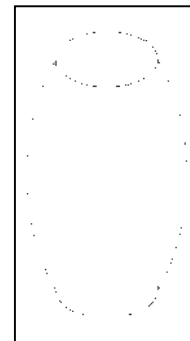
SPECIFIC GRAVITY OF SOLIDS: 2.75 (Assumed)

LOAD CELL NO.:

INITIAL SAMPLE DATA	
AVERAGE DIAMETER (in.):	2.87
HEIGHT (in.):	6.07
HEIGHT TO DIAMETER RATIO:	2.11
WET UNIT WEIGHT (pcf):	127.2
DRY UNIT WEIGHT (pcf):	103.9
VOID RATIO:	0.65
MOISTURE CONTENT (%)*:	22.5
DEGREE OF SATURATION (%):	94.8

FAILURE DATA***	
MOISTURE CONTENT AFTER FAILURE (%)**:	22.7
AVERAGE RATE OF AXIAL STRAIN TO FAILURE (%/min.):	1.0
AXIAL STRAIN AT FAILURE (%):	14.9
PRINCIPAL STRESS DIFFERENCE AT FAILURE, $\sigma_1 - \sigma_3$ (psi):	29.5
MINOR PRINCIPAL STRESS AT FAILURE, σ_3 (psi):	4.1
MAJOR PRINCIPAL STRESS AT FAILURE, σ_1 (psi):	33.6
UNDRAINED COMPRESSIVE STRENGTH, U_u (psf):	4,250
UNDRAINED SHEAR STRENGTH, s_u (psf):	2,125
LIMITING UNDRAINED COMP. STRESS @ 10% STRAIN (psf):	4,055

FAILURE SHAPES



REMARKS :

* Initial moisture content determined from sample cuttings.
 ** Final moisture content determined from entire sample.
 *** Failure stress values have been corrected for membrane effects.

UNCONSOLIDATED-UNDRAINED TRIAXIAL COMPRESSION TEST ON COHESIVE SOILS ASTM D2850

CLIENT : Fisher Arnold
 PROJECT NO.: J042140.01
 PROJECT: SR-222 Widening
 LOCATION: Haywood County, Tennessee

DATE: 2/4/2023

BORING NO.: SP-9	SAMPLE NO.: ST-2	DEPTH (ft.): 3.0-5.0
SAMPLE OBTAINED BY: Shelby Tube	CONDITION: Undisturbed	
SAMPLE DESCRIPTION: Medium stiff, brown, LEAN CLAY - (CL)		

LIQUID LIMIT (%): 43 PLASTIC LIMIT (%): 20 PLASTICITY INDEX (%): 23 USCS: CL

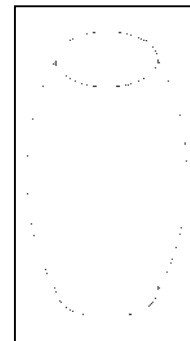
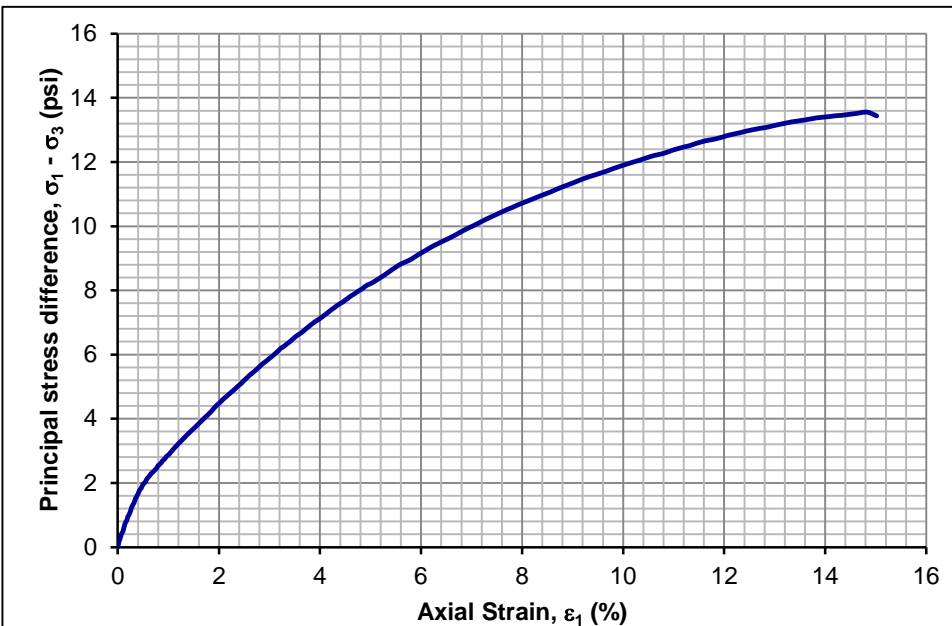
SPECIFIC GRAVITY OF SOLIDS: 2.75 (Assumed)

LOAD CELL NO.:

INITIAL SAMPLE DATA	
AVERAGE DIAMETER (in.):	2.83
HEIGHT (in.):	6.12
HEIGHT TO DIAMETER RATIO:	2.16
WET UNIT WEIGHT (pcf):	124.8
DRY UNIT WEIGHT (pcf):	100.3
VOID RATIO:	0.71
MOISTURE CONTENT (%)*:	24.4
DEGREE OF SATURATION (%):	94.5

FAILURE DATA***	
MOISTURE CONTENT AFTER FAILURE (%)**:	14.5
AVERAGE RATE OF AXIAL STRAIN TO FAILURE (%/min.):	1.0
AXIAL STRAIN AT FAILURE (%):	14.8
PRINCIPAL STRESS DIFFERENCE AT FAILURE, $\sigma_1 - \sigma_3$ (psi):	13.6
MINOR PRINCIPAL STRESS AT FAILURE, σ_3 (psi):	2.3
MAJOR PRINCIPAL STRESS AT FAILURE, σ_1 (psi):	15.9
UNDRAINED COMPRESSIVE STRENGTH, U_u (psf):	1,950
UNDRAINED SHEAR STRENGTH, s_u (psf):	975
LIMITING UNDRAINED COMP. STRESS @ 10% STRAIN (psf):	1,715

FAILURE SHAPES



REMARKS :

* Initial moisture content determined from sample cuttings.

** Final moisture content determined from entire sample.

*** Failure stress values have been corrected for membrane effects.

UNCONSOLIDATED-UNDRAINED TRIAXIAL COMPRESSION TEST ON COHESIVE SOILS ASTM D2850

CLIENT : Fisher Arnold
 PROJECT NO.: J042140.01
 PROJECT: SR-222 Widening
 LOCATION: Haywood County, Tennessee

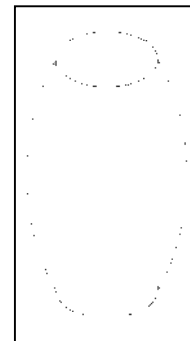
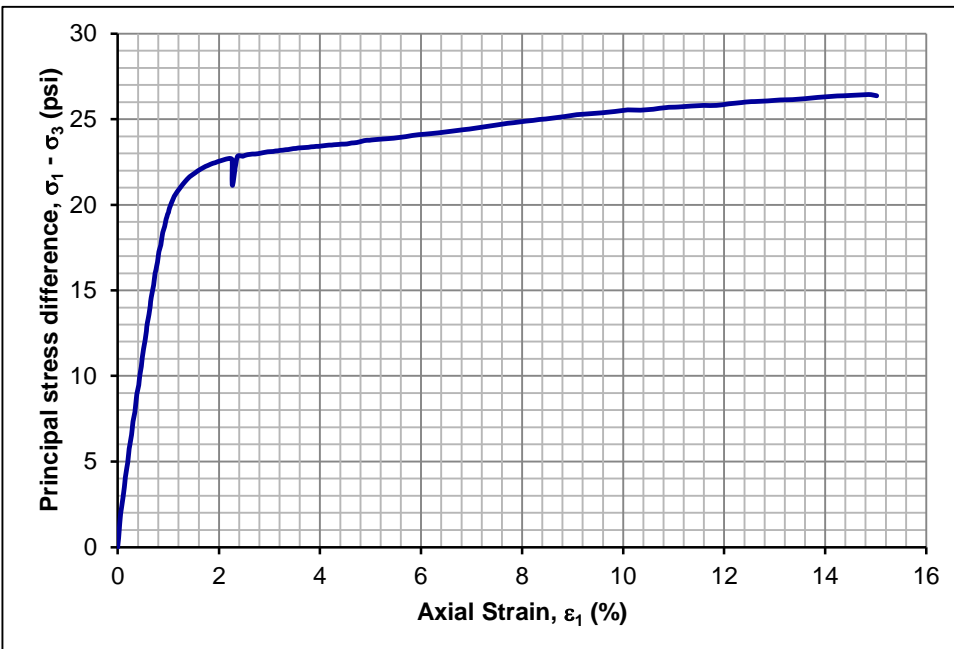
DATE: 2/3/2023

BORING NO.: SP-10	SAMPLE NO.: ST-2	DEPTH (ft.): 3.0-5.0
SAMPLE OBTAINED BY: Shelby Tube	CONDITION: Undisturbed	
SAMPLE DESCRIPTION: Stiff, brown, FAT CLAY - (CH)		

LIQUID LIMIT (%): 65 PLASTIC LIMIT (%): 19 PLASTICITY INDEX (%): 46 USCS: CH

SPECIFIC GRAVITY OF SOLIDS: 2.75 (Assumed) LOAD CELL NO.:

INITIAL SAMPLE DATA	FAILURE DATA***
AVERAGE DIAMETER (in.): 2.87	MOISTURE CONTENT AFTER FAILURE (%)**: 23.2
HEIGHT (in.): 5.93	AVERAGE RATE OF AXIAL STRAIN TO FAILURE (%/min.): 1.0
HEIGHT TO DIAMETER RATIO: 2.07	AXIAL STRAIN AT FAILURE (%): 14.9
WET UNIT WEIGHT (pcf): 130.3	PRINCIPAL STRESS DIFFERENCE AT FAILURE, $\sigma_1 - \sigma_3$ (psi): 26.4
DRY UNIT WEIGHT (pcf): 106.6	MINOR PRINCIPAL STRESS AT FAILURE, σ_3 (psi): 2.3
VOID RATIO: 0.61	MAJOR PRINCIPAL STRESS AT FAILURE, σ_1 (psi): 28.8
MOISTURE CONTENT (%)*: 22.2	UNDRAINED COMPRESSIVE STRENGTH, U_u (psf): 3,810
DEGREE OF SATURATION (%): 100.0	UNDRAINED SHEAR STRENGTH, s_u (psf): 1,905
	LIMITING UNDRAINED COMP. STRESS @ 10% STRAIN (psf): 3,675



REMARKS :

* Initial moisture content determined from sample cuttings.
 ** Final moisture content determined from entire sample.
 *** Failure stress values have been corrected for membrane effects.

UNCONSOLIDATED-UNDRAINED TRIAXIAL COMPRESSION TEST ON COHESIVE SOILS ASTM D2850

CLIENT : Fisher Arnold
 PROJECT NO.: J042140.01
 PROJECT: SR-222 Widening
 LOCATION: Haywood County, Tennessee

DATE: 1/19/2023

BORING NO.: W-1A
 SAMPLE OBTAINED BY: Shelby Tube
 SAMPLE DESCRIPTION: Stiff, brown, FAT CLAY - (CH)

SAMPLE NO.: ST-4
 CONDITION: Undisturbed

DEPTH (ft.): 8.0-10.0

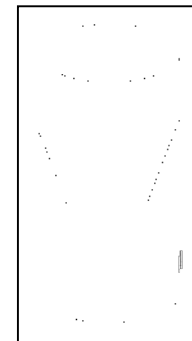
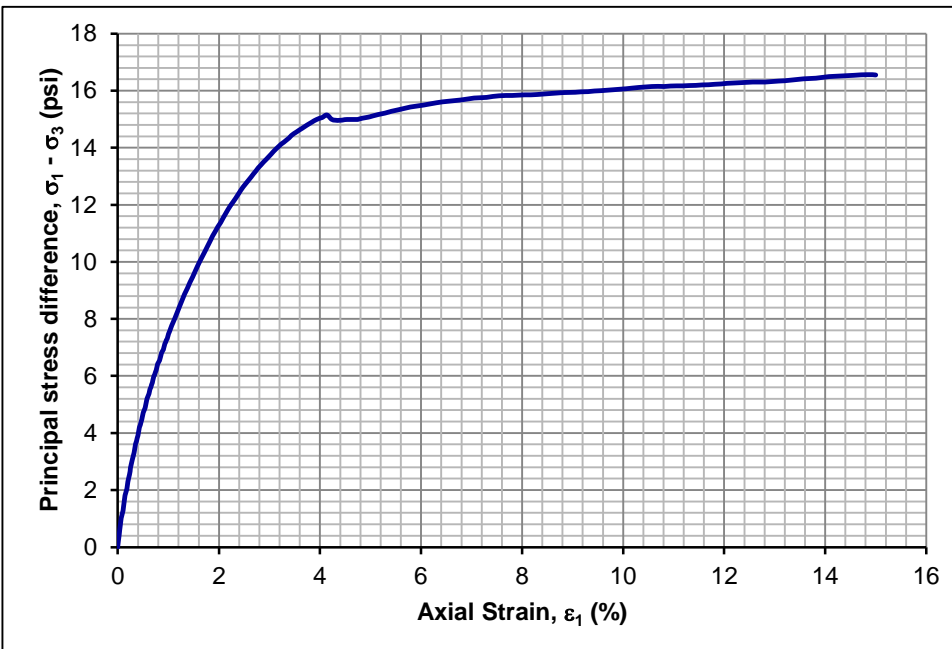
LIQUID LIMIT (%): 59 PLASTIC LIMIT (%): 19 PLASTICITY INDEX (%): 40 USCS: CH

SPECIFIC GRAVITY OF SOLIDS: 2.75 (Assumed)

LOAD CELL NO.:

INITIAL SAMPLE DATA	
AVERAGE DIAMETER (in.):	2.85
HEIGHT (in.):	6.00
HEIGHT TO DIAMETER RATIO:	2.11
WET UNIT WEIGHT (pcf):	125.4
DRY UNIT WEIGHT (pcf):	101.7
VOID RATIO:	0.69
MOISTURE CONTENT (%)*:	23.3
DEGREE OF SATURATION (%):	93.3

FAILURE DATA***	
MOISTURE CONTENT AFTER FAILURE (%)**:	26.5
AVERAGE RATE OF AXIAL STRAIN TO FAILURE (%/min.):	1.0
AXIAL STRAIN AT FAILURE (%):	14.8
PRINCIPAL STRESS DIFFERENCE AT FAILURE, $\sigma_1 - \sigma_3$ (psi):	16.6
MINOR PRINCIPAL STRESS AT FAILURE, σ_3 (psi):	5.3
MAJOR PRINCIPAL STRESS AT FAILURE, σ_1 (psi):	21.8
UNDRAINED COMPRESSIVE STRENGTH, U_u (psf):	2,390
UNDRAINED SHEAR STRENGTH, s_u (psf):	1,195
LIMITING UNDRAINED COMP. STRESS @ 10% STRAIN (psf):	2,315



REMARKS :

* Initial moisture content determined from sample cuttings.

** Final moisture content determined from entire sample.

*** Failure stress values have been corrected for membrane effects.

UNCONSOLIDATED-UNDRAINED TRIAXIAL COMPRESSION TEST ON COHESIVE SOILS ASTM D2850

CLIENT : Fisher Arnold
 PROJECT NO.: J042140.01
 PROJECT: SR-222 Widening
 LOCATION: Haywood County, Tennessee

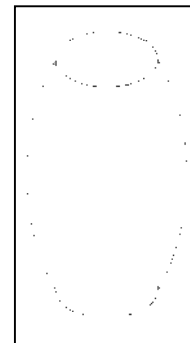
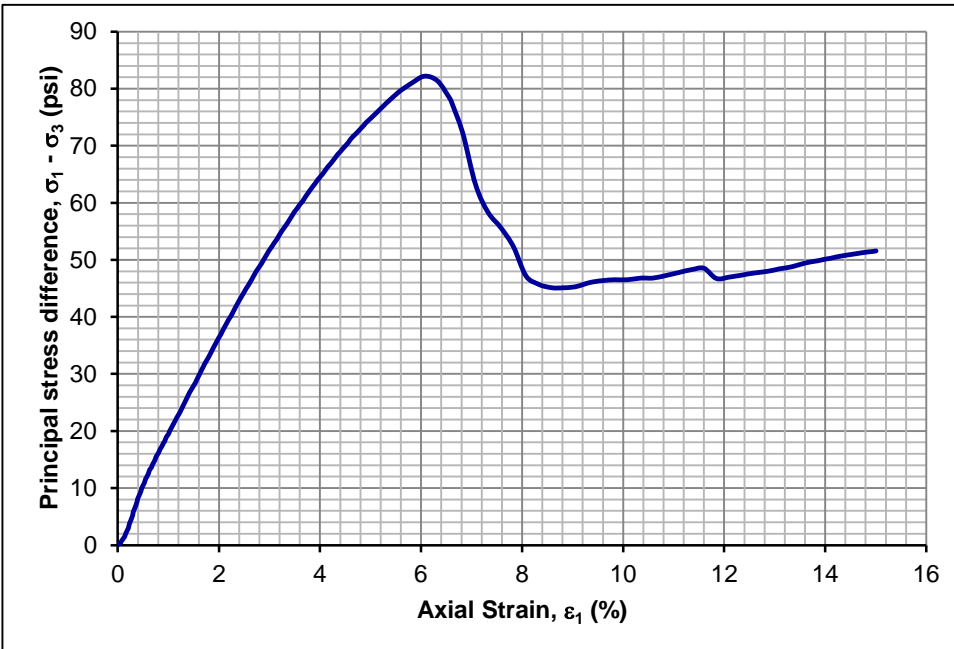
DATE: 1/19/2023

BORING NO.: W-1B	SAMPLE NO.: ST-2	DEPTH (ft.): 3.0-5.0
SAMPLE OBTAINED BY: Shelby Tube	CONDITION: Undisturbed	
SAMPLE DESCRIPTION: Hard, brown, LEAN CLAY - (CL)		

LIQUID LIMIT (%): 47 PLASTIC LIMIT (%): 23 PLASTICITY INDEX (%): 24 USCS: CL

SPECIFIC GRAVITY OF SOLIDS: 2.75 (Assumed) LOAD CELL NO.:

INITIAL SAMPLE DATA	FAILURE DATA***
AVERAGE DIAMETER (in.): 2.86	MOISTURE CONTENT AFTER FAILURE (%)**: 19.5
HEIGHT (in.): 5.65	AVERAGE RATE OF AXIAL STRAIN TO FAILURE (%/min.): 1.0
HEIGHT TO DIAMETER RATIO: 1.97	AXIAL STRAIN AT FAILURE (%): 6.1
WET UNIT WEIGHT (pcf): 129.2	PRINCIPAL STRESS DIFFERENCE AT FAILURE, $\sigma_1 - \sigma_3$ (psi): 82.2
DRY UNIT WEIGHT (pcf): 118.2	MINOR PRINCIPAL STRESS AT FAILURE, σ_3 (psi): 2.3
VOID RATIO: 0.45	MAJOR PRINCIPAL STRESS AT FAILURE, σ_1 (psi): 84.5
MOISTURE CONTENT (%)*: 9.3	UNDRAINED COMPRESSIVE STRENGTH, U_u (psf): 11,830
DEGREE OF SATURATION (%): 56.7	UNDRAINED SHEAR STRENGTH, s_u (psf): 5,915
	LIMITING UNDRAINED COMP. STRESS @ 10% STRAIN (psf): N/A



REMARKS :

* Initial moisture content determined from sample cuttings.
 ** Final moisture content determined from entire sample.
 *** Failure stress values have been corrected for membrane effects.

UNCONSOLIDATED-UNDRAINED TRIAXIAL COMPRESSION TEST ON COHESIVE SOILS ASTM D2850

CLIENT : Fisher Arnold
 PROJECT NO.: J042140.01
 PROJECT: SR-222 Widening
 LOCATION: Haywood County, Tennessee

DATE: 1/19/2023

BORING NO.: W-2
 SAMPLE OBTAINED BY: Shelby Tube
 SAMPLE DESCRIPTION: Stiff, brown, LEAN CLAY - (CL)

SAMPLE NO.: ST-16
 CONDITION: Undisturbed

DEPTH (ft.): 18.0-20.0

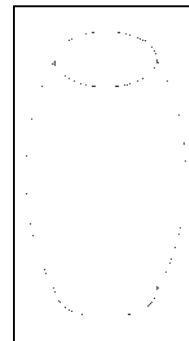
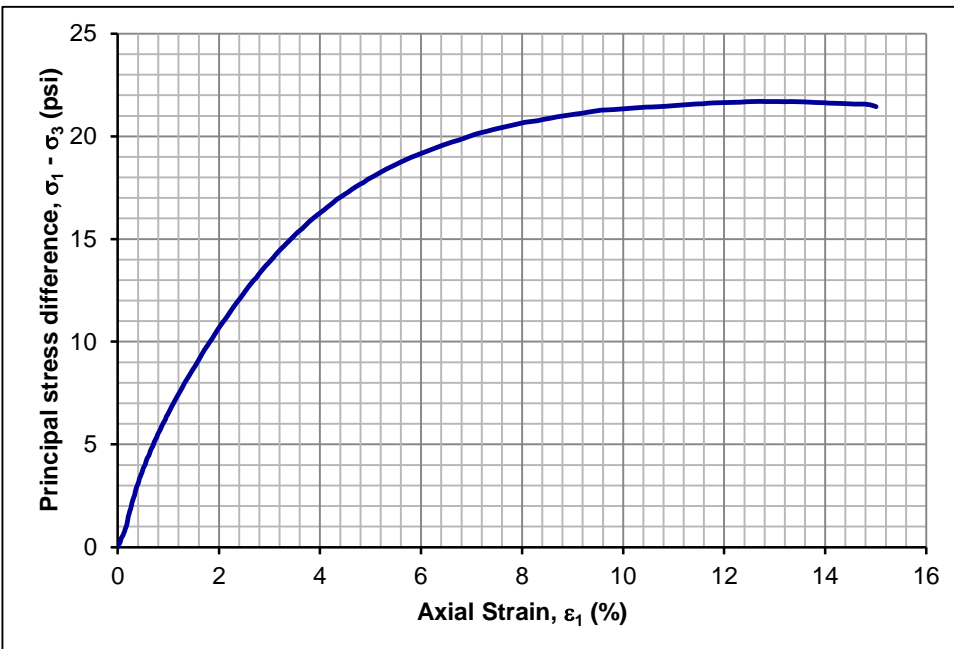
LIQUID LIMIT (%): 46 PLASTIC LIMIT (%): 16 PLASTICITY INDEX (%): 30 USCS: CL

SPECIFIC GRAVITY OF SOLIDS: 2.75 (Assumed)

LOAD CELL NO.:

INITIAL SAMPLE DATA		FAILURE DATA***	
AVERAGE DIAMETER (in.):	2.87	MOISTURE CONTENT AFTER FAILURE (%)**:	25.6
HEIGHT (in.):	5.62	AVERAGE RATE OF AXIAL STRAIN TO FAILURE (%/min.):	1.0
HEIGHT TO DIAMETER RATIO:	1.96	AXIAL STRAIN AT FAILURE (%):	12.8
WET UNIT WEIGHT (pcf):	120.0	PRINCIPAL STRESS DIFFERENCE AT FAILURE, $\sigma_1 - \sigma_3$ (psi):	21.7
DRY UNIT WEIGHT (pcf):	97.7	MINOR PRINCIPAL STRESS AT FAILURE, σ_3 (psi):	11.1
VOID RATIO:	0.76	MAJOR PRINCIPAL STRESS AT FAILURE, σ_1 (psi):	32.8
MOISTURE CONTENT (%)*:	22.9	UNDRAINED COMPRESSIVE STRENGTH, U_u (psf):	3,120
DEGREE OF SATURATION (%):	83.1	UNDRAINED SHEAR STRENGTH, s_u (psf):	1,560
		LIMITING UNDRAINED COMP. STRESS @ 10% STRAIN (psf):	3,075

FAILURE SHAPES



REMARKS :

* Initial moisture content determined from sample cuttings.

** Final moisture content determined from entire sample.

*** Failure stress values have been corrected for membrane effects.

UNCONSOLIDATED-UNDRAINED TRIAXIAL COMPRESSION TEST ON COHESIVE SOILS ASTM D2850

CLIENT : Fisher Arnold
 PROJECT NO.: J042140.01
 PROJECT: SR-222 Widening
 LOCATION: Haywood County, Tennessee

DATE: 1/23/2023

BORING NO.: W-3A
 SAMPLE OBTAINED BY: Shelby Tube
 SAMPLE DESCRIPTION: Stiff, brown, sandy, FAT CLAY - (CH)

SAMPLE NO.: ST-7
 CONDITION: Undisturbed

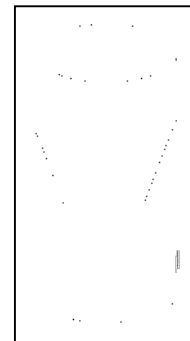
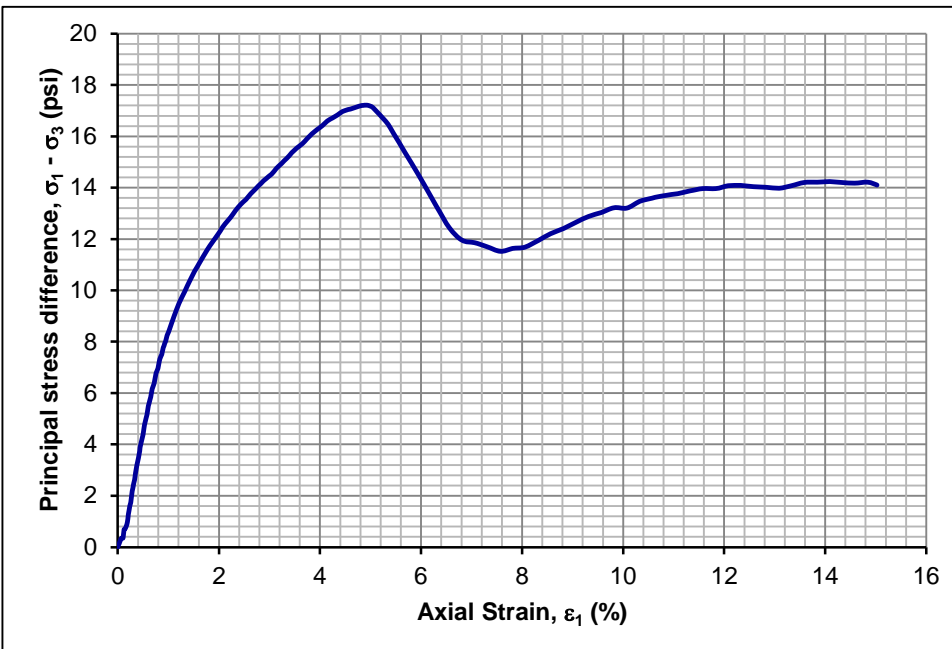
DEPTH (ft.): 23.0-25.0

LIQUID LIMIT (%): 79 PLASTIC LIMIT (%): 26 PLASTICITY INDEX (%): 53 USCS: CH

SPECIFIC GRAVITY OF SOLIDS: 2.75 (Assumed)

LOAD CELL NO.:

INITIAL SAMPLE DATA		FAILURE DATA***	
AVERAGE DIAMETER (in.):	2.86	MOISTURE CONTENT AFTER FAILURE (%)**:	41.6
HEIGHT (in.):	5.87	AVERAGE RATE OF AXIAL STRAIN TO FAILURE (%/min.):	1.0
HEIGHT TO DIAMETER RATIO:	2.05	AXIAL STRAIN AT FAILURE (%):	4.9
WET UNIT WEIGHT (pcf):	111.3	PRINCIPAL STRESS DIFFERENCE AT FAILURE, $\sigma_1 - \sigma_3$ (psi):	17.2
DRY UNIT WEIGHT (pcf):	83.5	MINOR PRINCIPAL STRESS AT FAILURE, σ_3 (psi):	14.0
VOID RATIO:	1.05	MAJOR PRINCIPAL STRESS AT FAILURE, σ_1 (psi):	31.2
MOISTURE CONTENT (%)*:	33.2	UNDRAINED COMPRESSIVE STRENGTH, U_u (psf):	2,480
DEGREE OF SATURATION (%):	86.7	UNDRAINED SHEAR STRENGTH, s_u (psf):	1,240
		LIMITING UNDRAINED COMP. STRESS @ 10% STRAIN (psf):	N/A



REMARKS :

* Initial moisture content determined from sample cuttings.
 ** Final moisture content determined from entire sample.
 *** Failure stress values have been corrected for membrane effects.

UNCONSOLIDATED-UNDRAINED TRIAXIAL COMPRESSION TEST ON COHESIVE SOILS ASTM D2850

CLIENT : Fisher Arnold
 PROJECT NO.: J042140.01
 PROJECT: SR-222 Widening
 LOCATION: Haywood County, Tennessee

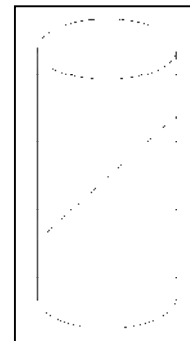
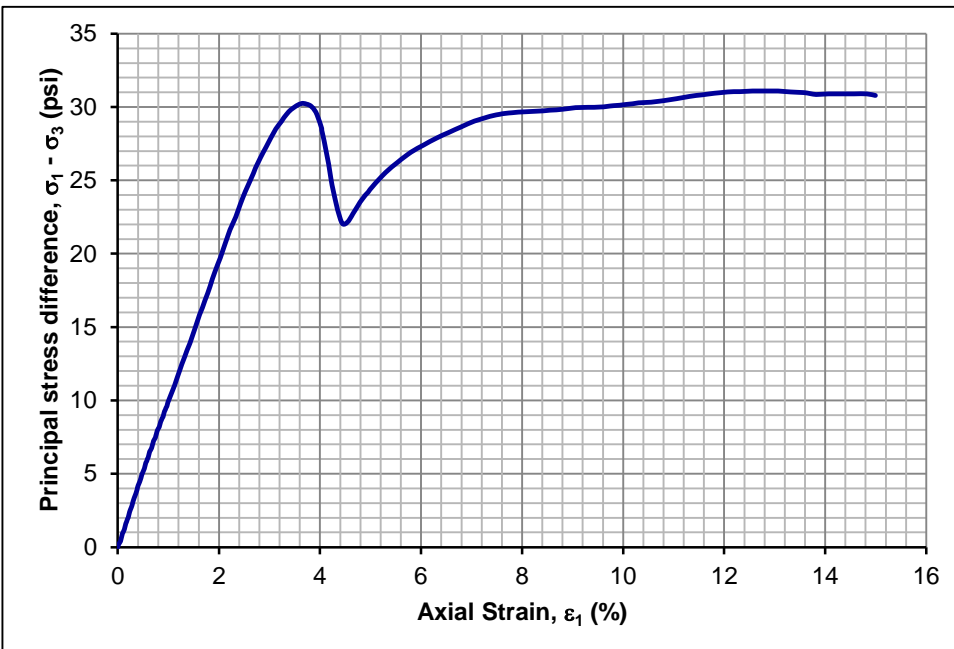
DATE: 1/25/2023

BORING NO.: W-8 SAMPLE NO.: ST-4 DEPTH (ft.): 8.0-10.0
 SAMPLE OBTAINED BY: Shelby Tube CONDITION: Undisturbed
 SAMPLE DESCRIPTION: Very stiff, brown, LEAN CLAY- (CL)

LIQUID LIMIT (%): 37 PLASTIC LIMIT (%): 23 PLASTICITY INDEX (%): 14 USCS: CL

SPECIFIC GRAVITY OF SOLIDS: 2.75 (Assumed) LOAD CELL NO.:

INITIAL SAMPLE DATA		FAILURE DATA***	
AVERAGE DIAMETER (in.):	2.83	MOISTURE CONTENT AFTER FAILURE (%)**:	23.0
HEIGHT (in.):	6.16	AVERAGE RATE OF AXIAL STRAIN TO FAILURE (%/min.):	1.0
HEIGHT TO DIAMETER RATIO:	2.18	AXIAL STRAIN AT FAILURE (%):	12.8
WET UNIT WEIGHT (pcf):	127.4	PRINCIPAL STRESS DIFFERENCE AT FAILURE, $\sigma_1 - \sigma_3$ (psi):	31.1
DRY UNIT WEIGHT (pcf):	104.3	MINOR PRINCIPAL STRESS AT FAILURE, σ_3 (psi):	5.3
VOID RATIO:	0.65	MAJOR PRINCIPAL STRESS AT FAILURE, σ_1 (psi):	36.4
MOISTURE CONTENT (%)*:	22.1	UNDRAINED COMPRESSIVE STRENGTH, U_u (psf):	4,480
DEGREE OF SATURATION (%):	94.3	UNDRAINED SHEAR STRENGTH, s_u (psf):	2,240
		LIMITING UNDRAINED COMP. STRESS @ 10% STRAIN (psf):	4,340



REMARKS :

* Initial moisture content determined from sample cuttings.
 ** Final moisture content determined from entire sample.
 *** Failure stress values have been corrected for membrane effects.

UNCONSOLIDATED-UNDRAINED TRIAXIAL COMPRESSION TEST ON COHESIVE SOILS ASTM D2850

CLIENT : Fisher Arnold
 PROJECT NO.: J042140.01
 PROJECT: SR-222 Widening
 LOCATION: Haywood County, Tennessee

DATE: 1/24/2023

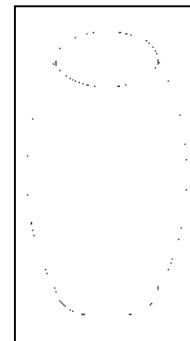
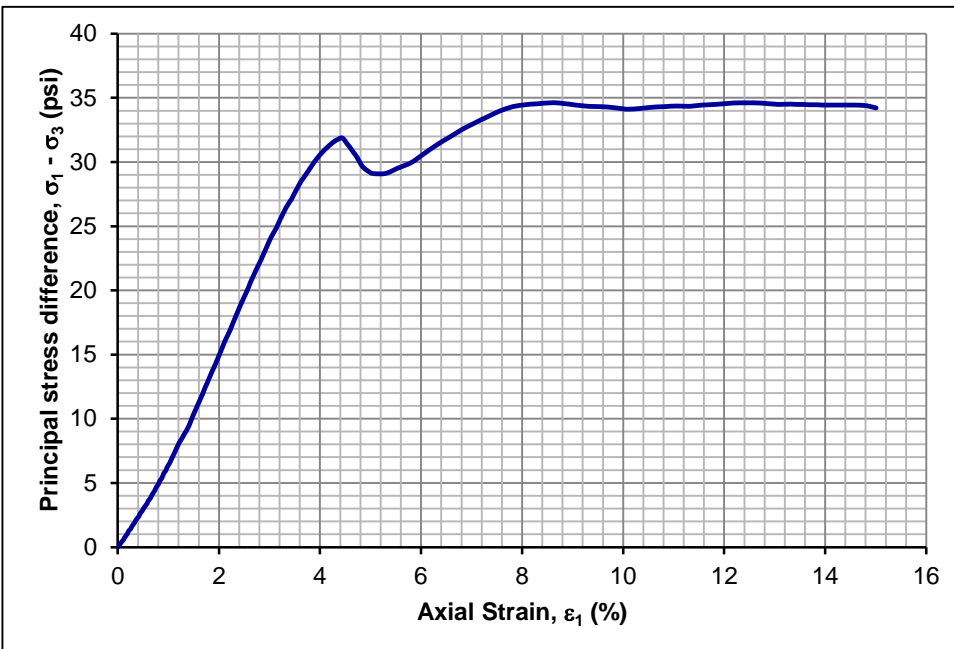
BORING NO.: W-10	SAMPLE NO.: ST-3	DEPTH (ft.): 3.0-5.0
SAMPLE OBTAINED BY: Shelby Tube	CONDITION: Undisturbed	
SAMPLE DESCRIPTION: Very stiff, brown, LEAN CLAY - (CL)		

LIQUID LIMIT (%): 40 PLASTIC LIMIT (%): 22 PLASTICITY INDEX (%): 18 USCS: CL

SPECIFIC GRAVITY OF SOLIDS: 2.75 (Assumed)

LOAD CELL NO.:

INITIAL SAMPLE DATA	FAILURE DATA***
AVERAGE DIAMETER (in.): 2.83	MOISTURE CONTENT AFTER FAILURE (%)**: 22.7
HEIGHT (in.): 6.19	AVERAGE RATE OF AXIAL STRAIN TO FAILURE (%/min.): 1.0
HEIGHT TO DIAMETER RATIO: 2.18	AXIAL STRAIN AT FAILURE (%): 8.6
WET UNIT WEIGHT (pcf): 131.6	PRINCIPAL STRESS DIFFERENCE AT FAILURE, $\sigma_1 - \sigma_3$ (psi): 34.6
DRY UNIT WEIGHT (pcf): 106.5	MINOR PRINCIPAL STRESS AT FAILURE, σ_3 (psi): 2.3
VOID RATIO: 0.61	MAJOR PRINCIPAL STRESS AT FAILURE, σ_1 (psi): 37.0
MOISTURE CONTENT (%)*: 23.6	UNDRAINED COMPRESSIVE STRENGTH, U_u (psf): 4,990
DEGREE OF SATURATION (%): 100.0	UNDRAINED SHEAR STRENGTH, s_u (psf): 2,495
	LIMITING UNDRAINED COMP. STRESS @ 10% STRAIN (psf): N/A



REMARKS :

* Initial moisture content determined from sample cuttings.
 ** Final moisture content determined from entire sample.
 *** Failure stress values have been corrected for membrane effects.

UNCONSOLIDATED-UNDRAINED TRIAXIAL COMPRESSION TEST ON COHESIVE SOILS ASTM D2850

CLIENT : Fisher Arnold
 PROJECT NO.: J042140.01
 PROJECT: SR-222 Widening
 LOCATION: Haywood County, Tennessee

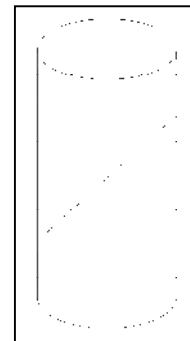
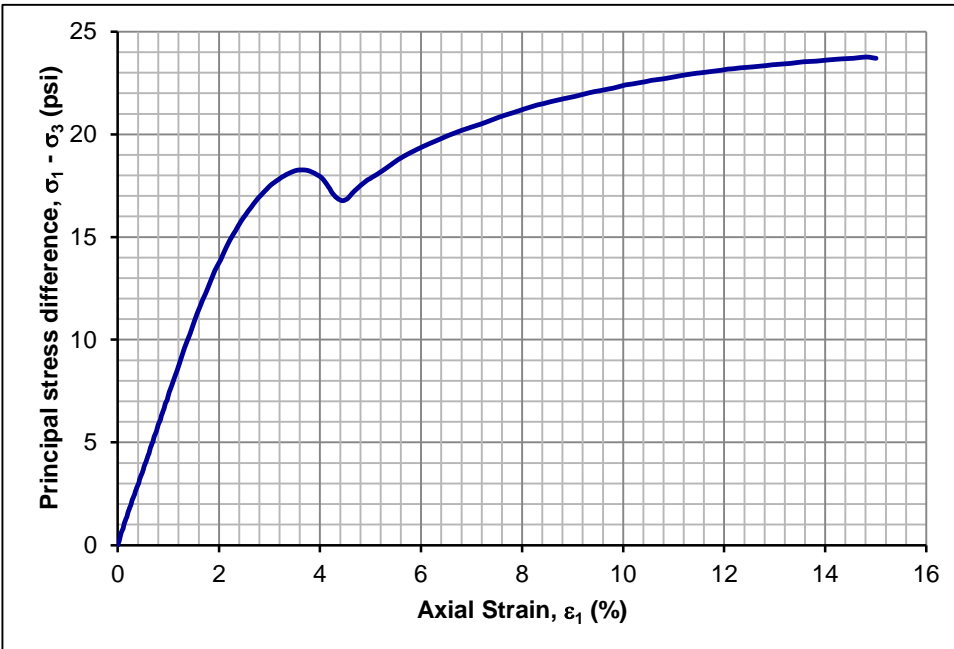
DATE: 2/20/2023

BORING NO.: W-14 SAMPLE NO.: ST-5 DEPTH (ft.): 10.0-12.0
 SAMPLE OBTAINED BY: Shelby Tube CONDITION: Undisturbed
 SAMPLE DESCRIPTION: Stiff, brown, LEAN CLAY - (CL)

LIQUID LIMIT (%): 43 PLASTIC LIMIT (%): 22 PLASTICITY INDEX (%): 21 USCS: CL

SPECIFIC GRAVITY OF SOLIDS: 2.75 (Assumed) LOAD CELL NO.:

INITIAL SAMPLE DATA		FAILURE DATA***	
AVERAGE DIAMETER (in.):	2.85	MOISTURE CONTENT AFTER FAILURE (%)**:	25.5
HEIGHT (in.):	6.11	AVERAGE RATE OF AXIAL STRAIN TO FAILURE (%/min.):	1.0
HEIGHT TO DIAMETER RATIO:	2.15	AXIAL STRAIN AT FAILURE (%):	14.8
WET UNIT WEIGHT (pcf):	124.6	PRINCIPAL STRESS DIFFERENCE AT FAILURE, $\sigma_1 - \sigma_3$ (psi):	23.8
DRY UNIT WEIGHT (pcf):	100.5	MINOR PRINCIPAL STRESS AT FAILURE, σ_3 (psi):	6.4
VOID RATIO:	0.71	MAJOR PRINCIPAL STRESS AT FAILURE, σ_1 (psi):	30.2
MOISTURE CONTENT (%)*:	24.0	UNDRAINED COMPRESSIVE STRENGTH, U_u (psf):	3,420
DEGREE OF SATURATION (%):	93.3	UNDRAINED SHEAR STRENGTH, s_u (psf):	1,710
		LIMITING UNDRAINED COMP. STRESS @ 10% STRAIN (psf):	3,220



REMARKS :

* Initial moisture content determined from sample cuttings.
 ** Final moisture content determined from entire sample.
 *** Failure stress values have been corrected for membrane effects.



TEST REPORT

Prepared For:
Fisher Arnold
9180 Crestwyn Hills Drive
Memphis, Tennessee 38125

Project No.: J042140.01
Project Name: SR 222 Improvement
Boring Number: BR-1
Sample ID: SS-9
Depth (ft): 38.5

January 20, 2023
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MINIMUM LABORATORY SOIL RESISTIVITY AASHTO T288

<u>Reading</u>	<u>Resistance Measurement</u>	<u>Soil Box Factor (cm)</u>	<u>Soil Resistivity (ohms-cm)</u>	<u>Moisture Content (%)</u>
#1	8,400	0.57	4,788.00	14.6
#2	3,400	0.57	1,938.00	21.9
#3	1,700	0.57	969.00	30.7

Minimum Soil Resistivity 969.00



TEST REPORT

Prepared For:
Fisher Arnold
9180 Crestwyn Hills Drive
Memphis, Tennessee 38125

Project No.: J042140.01
Project Name: SR 222 Improvement
Boring Number: BR-2
Sample ID: SS-5
Depth (ft): 13.5

January 20, 2023
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MINIMUM LABORATORY SOIL RESISTIVITY AASHTO T288

<u>Reading</u>	<u>Resistance Measurement</u>	<u>Soil Box Factor (cm)</u>	<u>Soil Resistivity (ohms-cm)</u>	<u>Moisture Content (%)</u>
#1	6,900	0.57	3,933.00	11.4
#2	3,700	0.57	2,109.00	18.8
#3	3,900	0.57	2,223.00	26.9
#4	4,600	0.57	2,622.00	35.2

Minimum Soil Resistivity **2,109.00**



TEST REPORT

Prepared For:
Fisher Arnold
9180 Crestwyn Hills Drive
Memphis, Tennessee 38125

Project No.: J042140.01
Project Name: SR 222 Improvement
Boring Number: BR-2
Sample ID: SS-7
Depth (ft): 23.5

January 20, 2023
Page 1 of 1

MINIMUM LABORATORY SOIL RESISTIVITY AASHTO T288

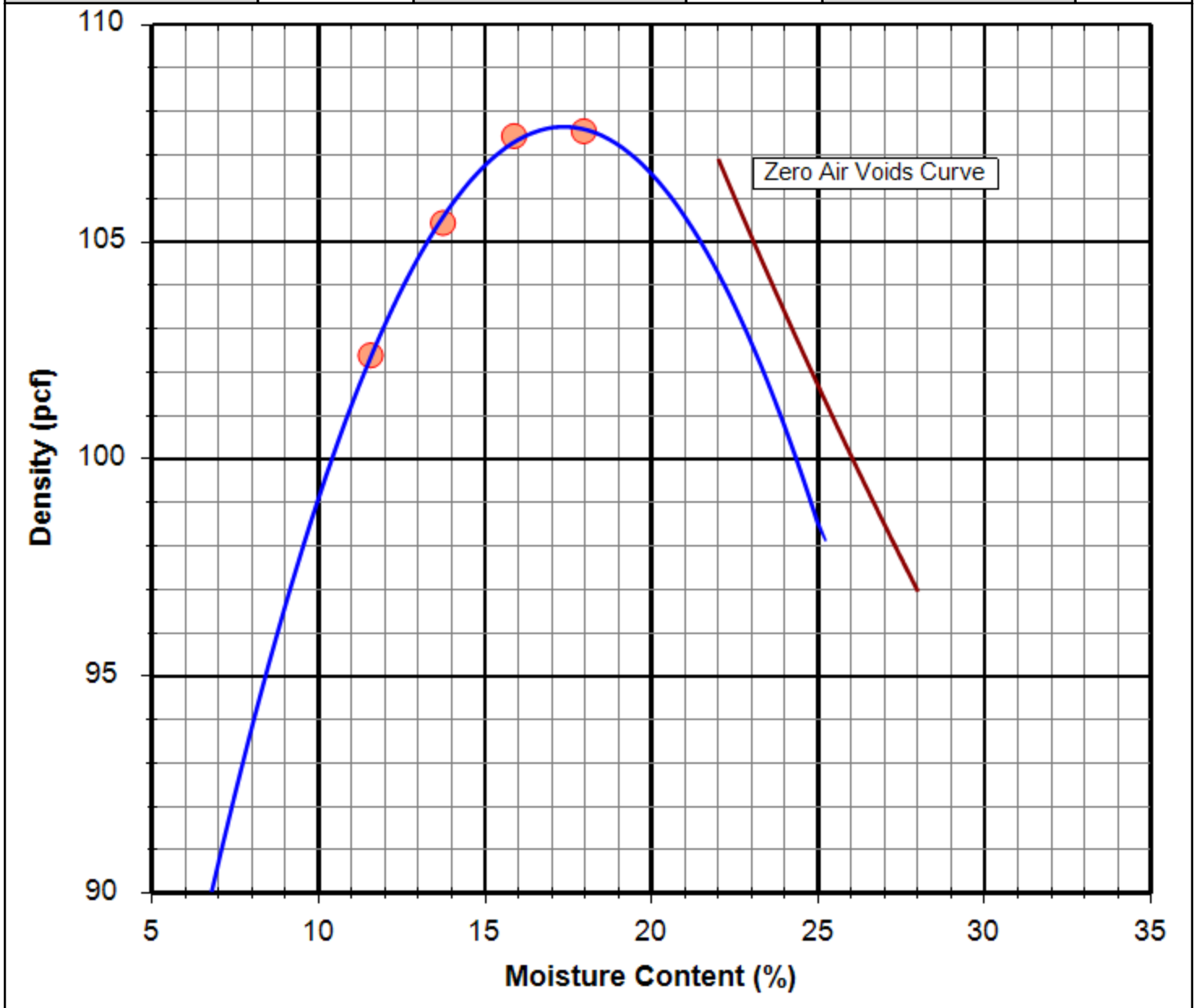
<u>Reading</u>	<u>Resistance Measurement</u>	<u>Soil Box Factor (cm)</u>	<u>Soil Resistivity (ohms-cm)</u>	<u>Moisture Content (%)</u>
#1	4,300	0.57	2,451.00	11.2
#2	3,200	0.57	1,824.00	18.4
#3	3,600	0.57	2,052.00	25.3

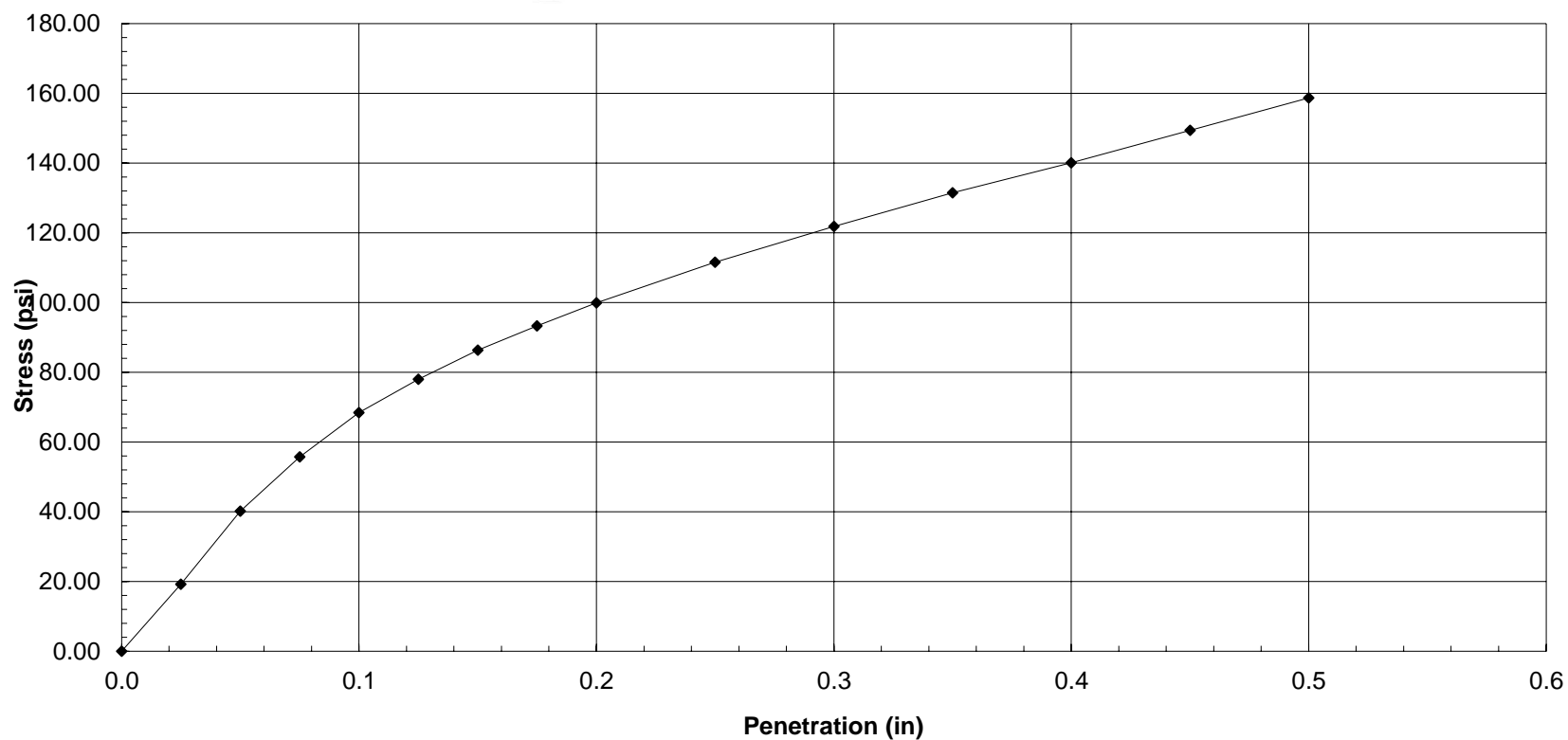
Minimum Soil Resistivity 1,824.00



STANDARD PROCTOR MOISTURE DENSITY TEST, ASTM D698, METHOD A

Client:	Fisher Arnold					Project No.:	J042140.01		
Project:	SR-222 Widening, Haywood County, TN					Date:	2/16/2023		
Sample Obtained From:	E-1					Depth (ft.):	1.0		
Sample Description:	Brown, silty, LEAN CLAY, trace sand - (CL) AASHTO A-6 (12)				LL	PL	PI	USCS	
					33	21	12	CL	
Maximum Dry Density (pcf):	107.7		Optimum Moisture Content:		17.5%		In Situ Moisture Content:		-





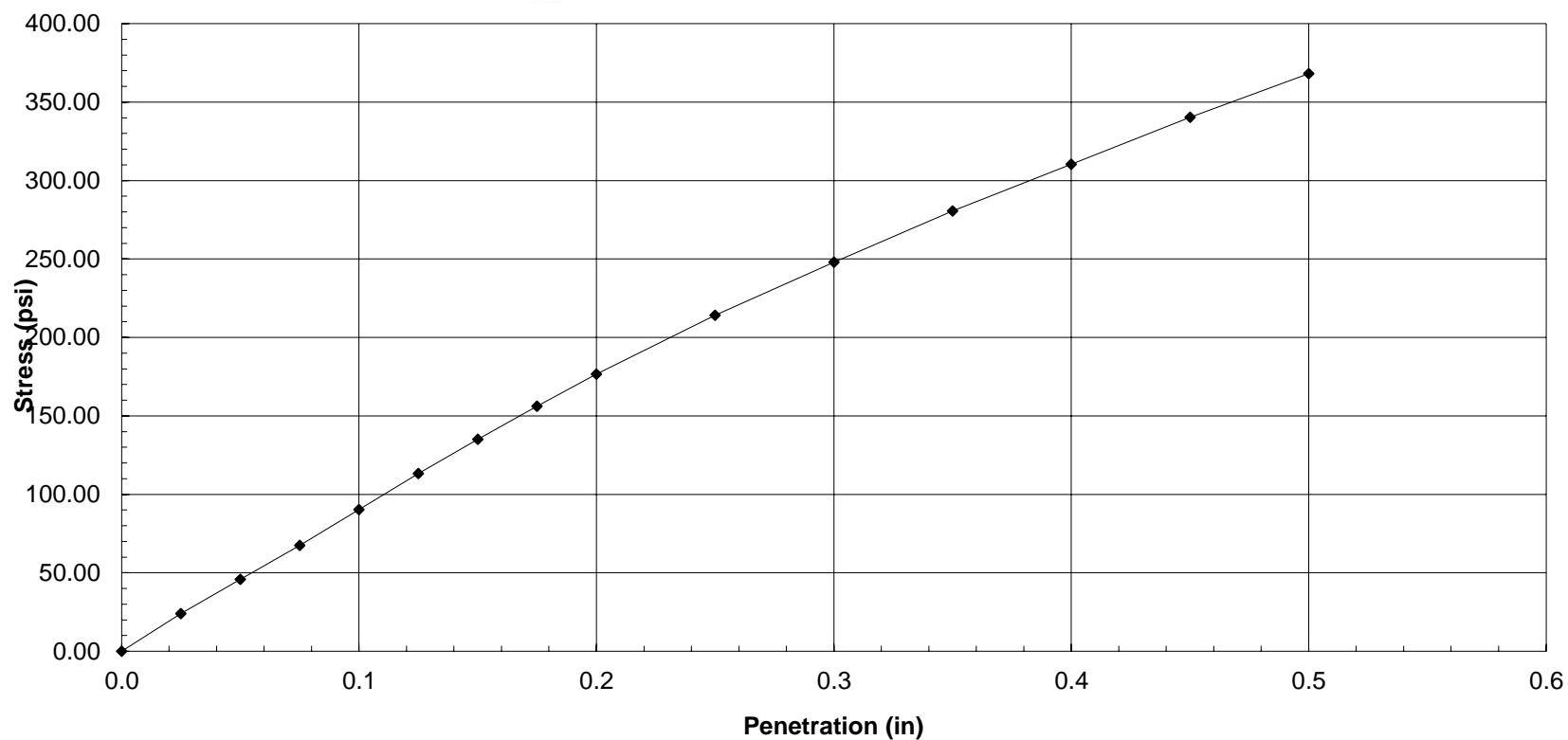
CALIFORNIA BEARING RATIO (CBR) TEST

ASTM D 1883

Project No.: J042140.01

Boring: E-1

Sample: 25 BLOWS - Depth: 1 ft.



CALIFORNIA BEARING RATIO (CBR) TEST

ASTM D 1883

Project No.: J042140.01

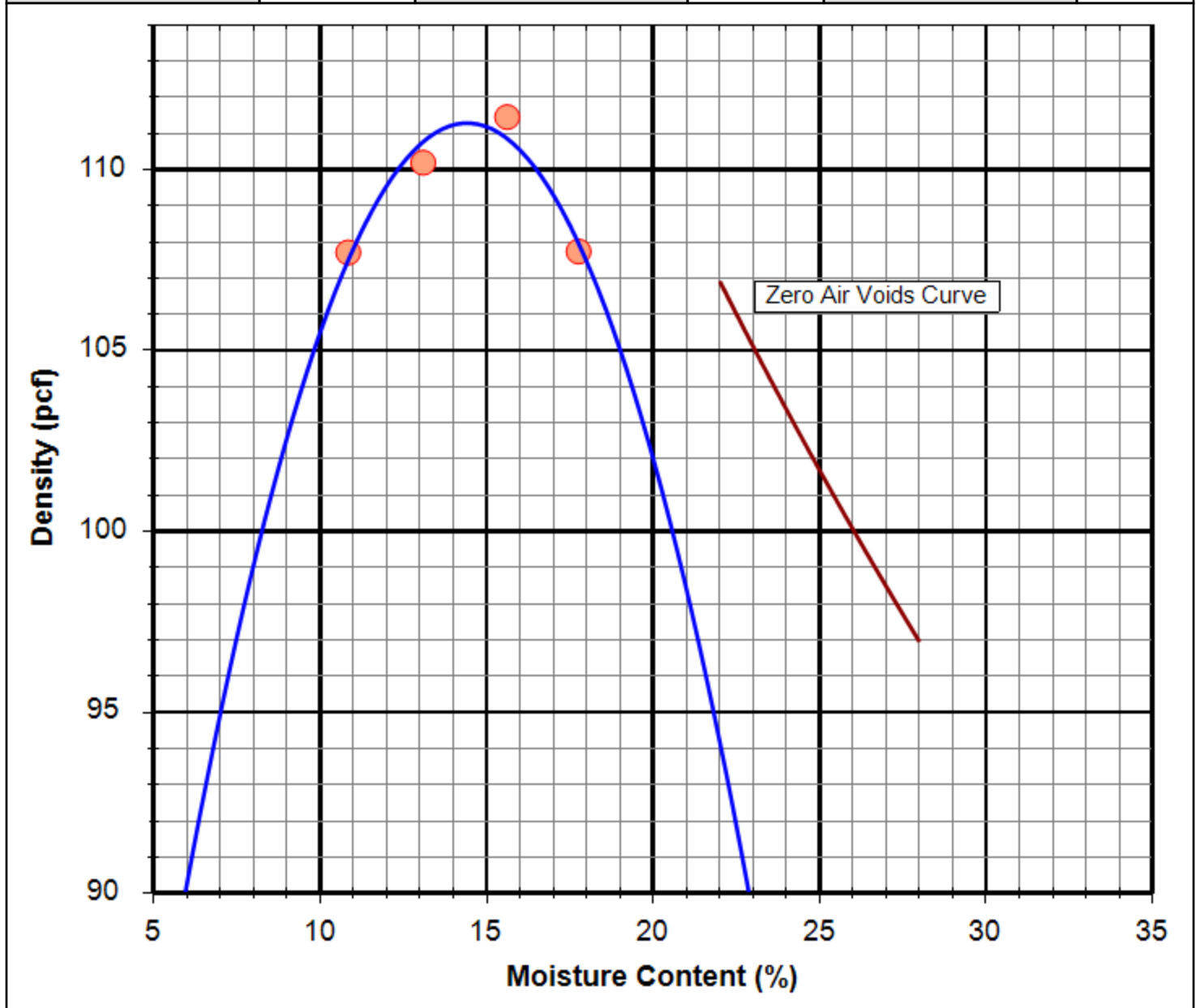
Boring: E-1

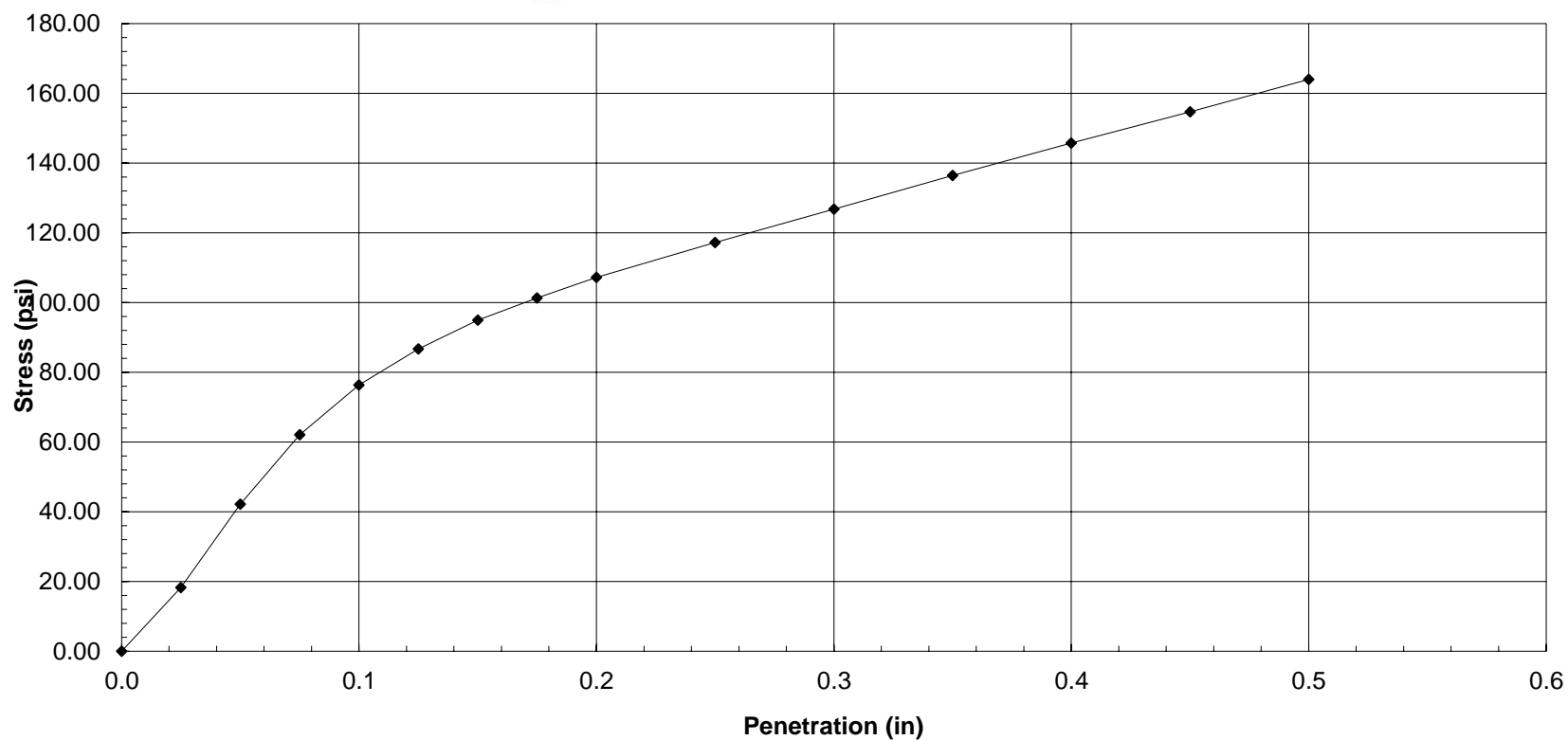
Sample: 56 BLOWS - Depth: 1 ft.



STANDARD PROCTOR MOISTURE DENSITY TEST, ASTM D698, METHOD A

Client:	Fisher Arnold					Project No.:	J042140.01		
Project:	SR-222 Widening, Haywood County, TN					Date:	2/15/2023		
Sample Obtained From:		E-14				Depth (ft.):	1.0		
Sample Description:		Brown, sandy, LEAN CLAY - (CL) AASHTO A-6 (7)			LL	PL	PI	USCS	
					33	21	12	CL	
Maximum Dry Density (pcf):		111.3	Optimum Moisture Content:		14.5%	In Situ Moisture Content:			-





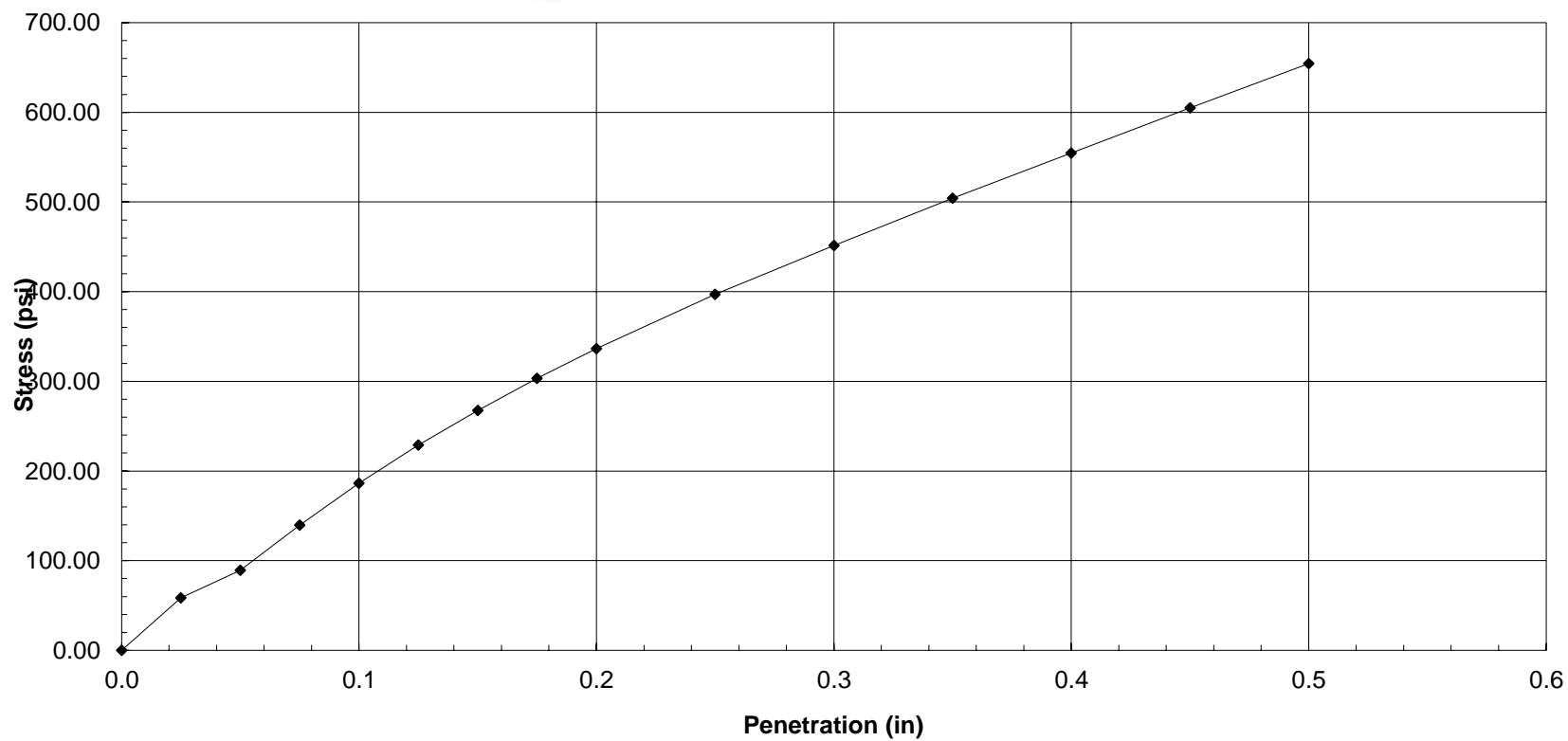
CALIFORNIA BEARING RATIO (CBR) TEST

ASTM D 1883

Project No.: J042140.01

Boring: E-14

Sample: 25 BLOWS - Depth: 1 ft.



CALIFORNIA BEARING RATIO (CBR) TEST

ASTM D 1883

Project No.: J042140.01

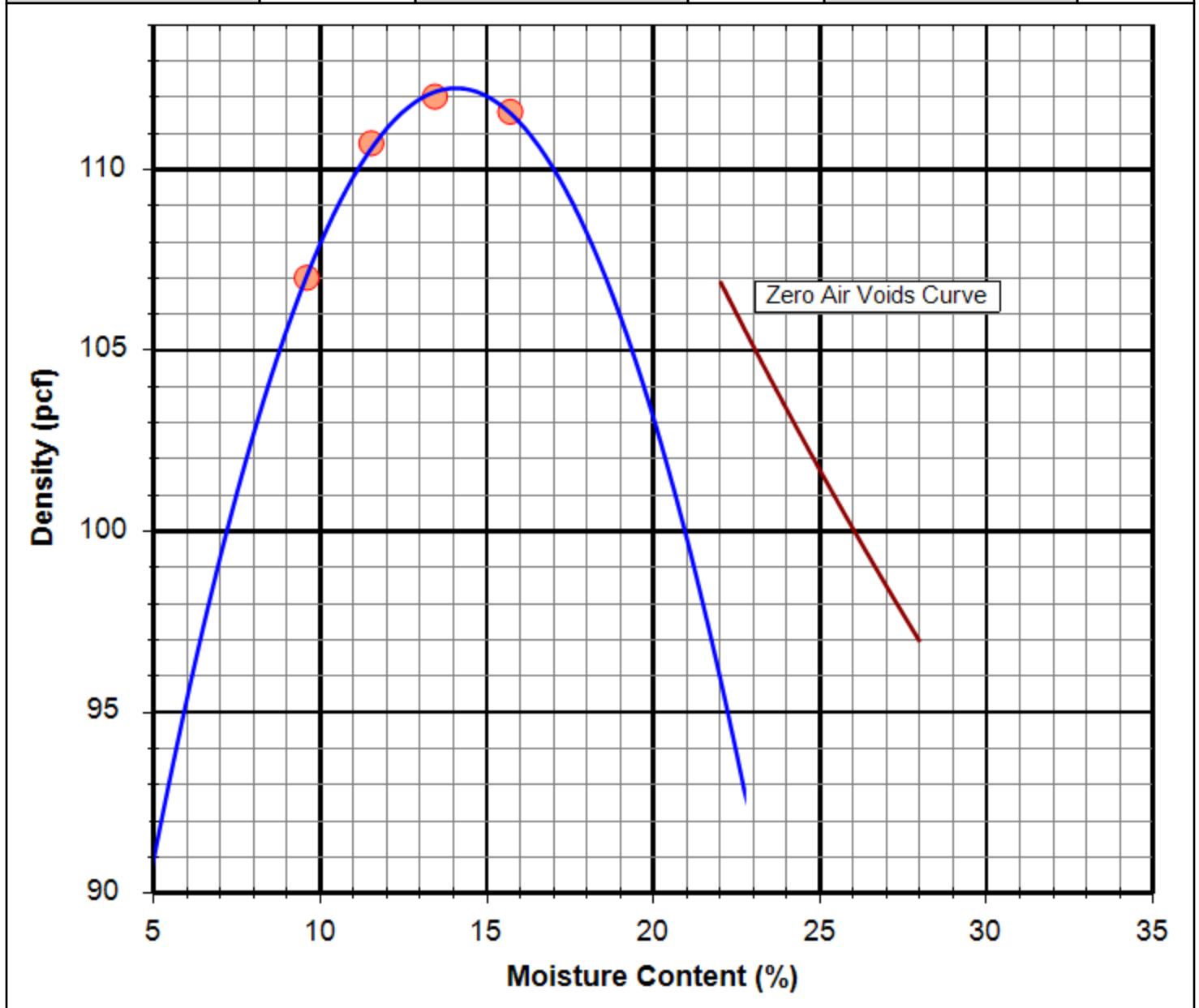
Boring: E-14

Sample: 56 BLOWS - Depth: 1 ft.



STANDARD PROCTOR MOISTURE DENSITY TEST, ASTM D698, METHOD A

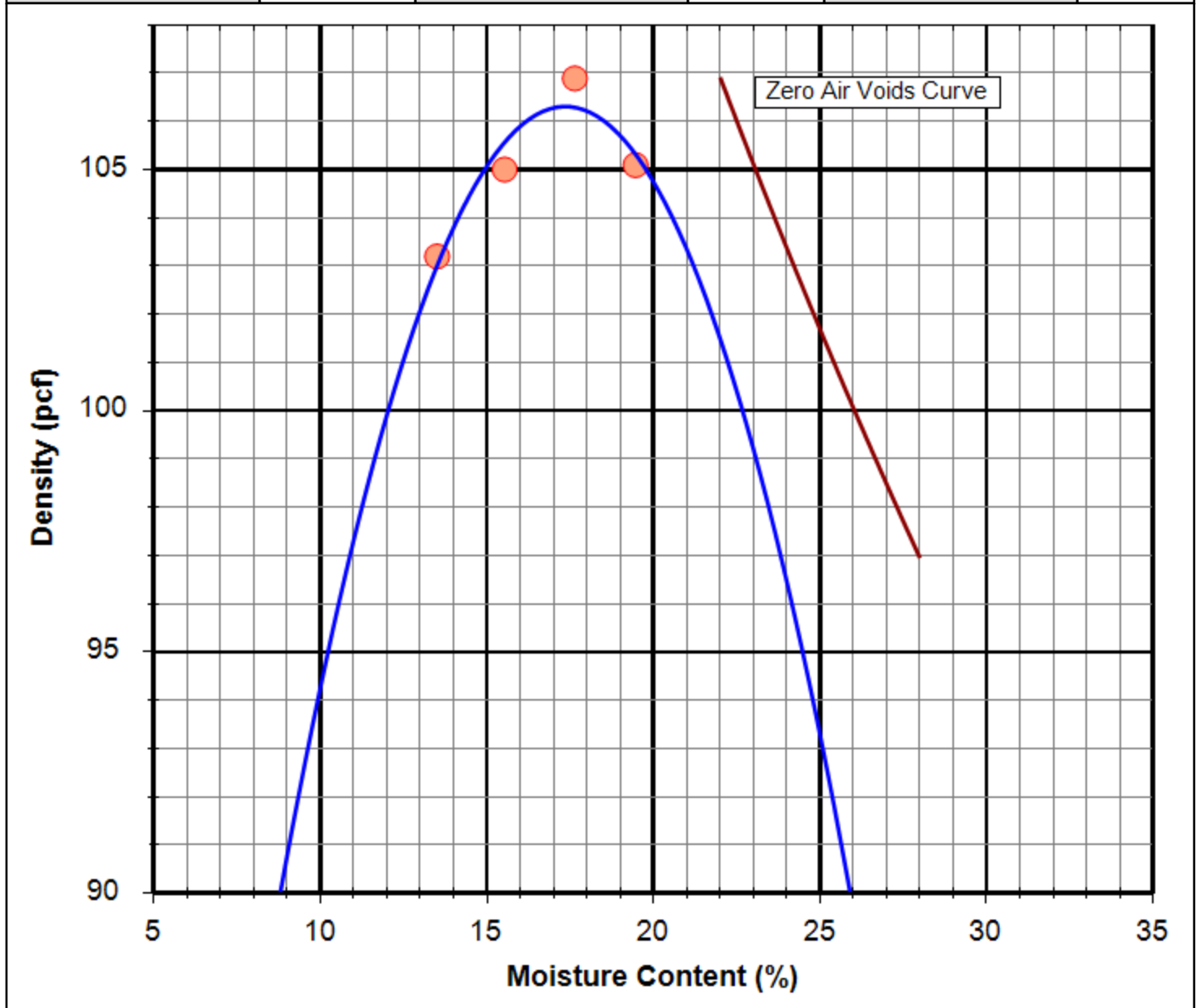
Client:	Fisher Arnold					Project No.:	J042140.01		
Project:	SR-222 Widening, Haywood County, TN					Date:	2/22/2023		
Sample Obtained From:		SP-3				Depth (ft.):	1.0		
Sample Description:		Brown and red, sandy, LEAN CLAY - (CL) AASHTO A-6 (10)			LL	PL	PI	USCS	
					38	15	23	CL	
Maximum Dry Density (pcf):		112.3	Optimum Moisture Content:		14.1%	In Situ Moisture Content:		-	





STANDARD PROCTOR MOISTURE DENSITY TEST, ASTM D698, METHOD A

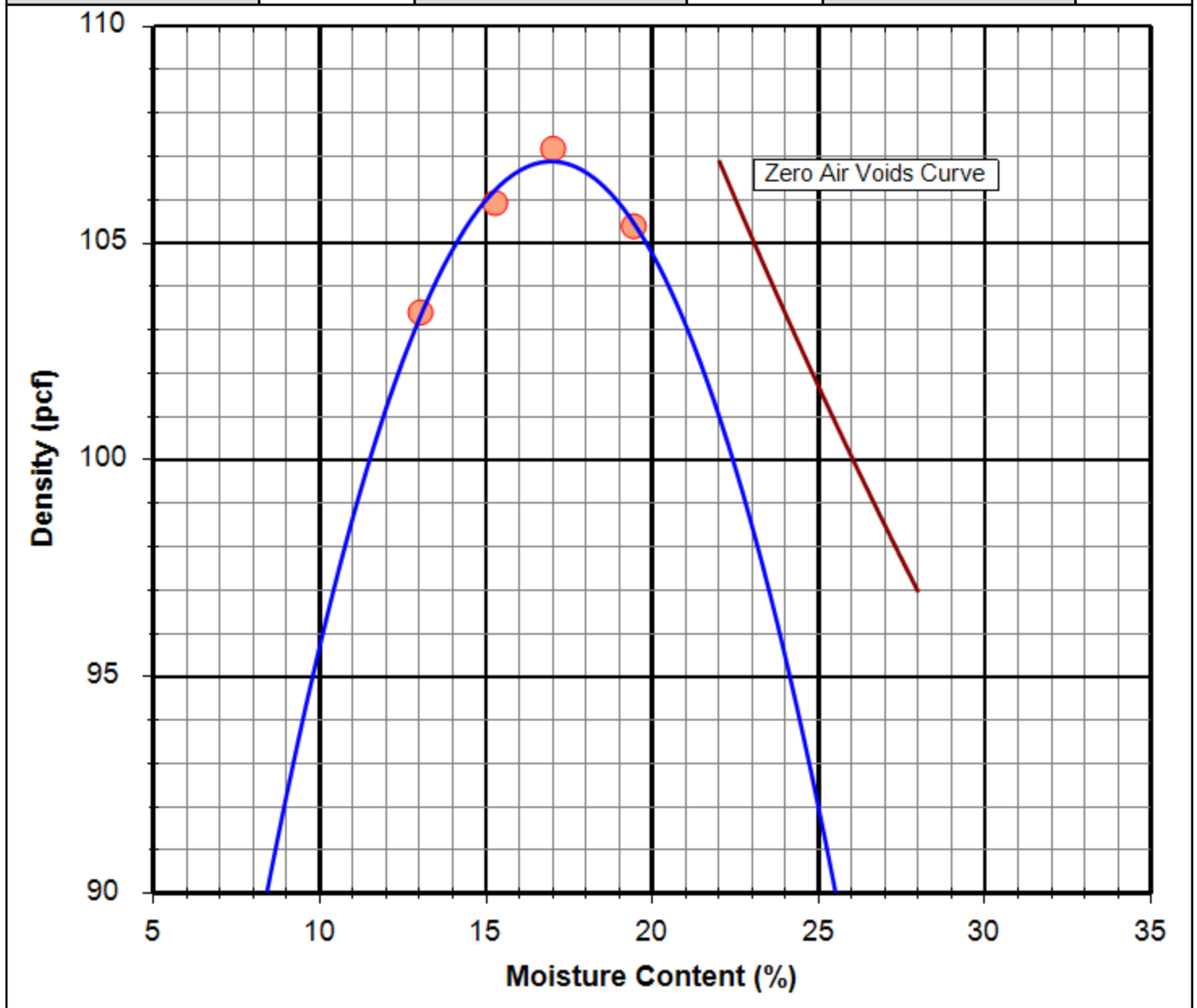
Client:	Fisher Arnold					Project No.:	J042140.01		
Project:	SR-222 Widening, Haywood County, TN					Date:	2/16/2023		
Sample Obtained From:		SP-6				Depth (ft.):	1.0		
Sample Description:		Brown, silty, LEAN CLAY - (CL) AASHTO A-6 (15)			LL	PL	PI	USCS	
					36	19	17	CL	
Maximum Dry Density (pcf):		106.3	Optimum Moisture Content:		17.3%	In Situ Moisture Content:		-	





STANDARD PROCTOR MOISTURE DENSITY TEST, ASTM D698, METHOD A

Client:	Fisher Arnold					Project No.:	J042140.01		
Project:	SR-222 Widening, Haywood County, TN					Date:	2/16/2023		
Sample Obtained From:		SP-10				Depth (ft.):	1.0		
Sample Description:		Brown, silty, LEAN CLAY - (CL) AASHTO A-6 (25)			LL	PL	PI	USCS	
					40	13	27	CL	
Maximum Dry Density (pcf):		106.9	Optimum Moisture Content:		16.9%	In Situ Moisture Content:		-	

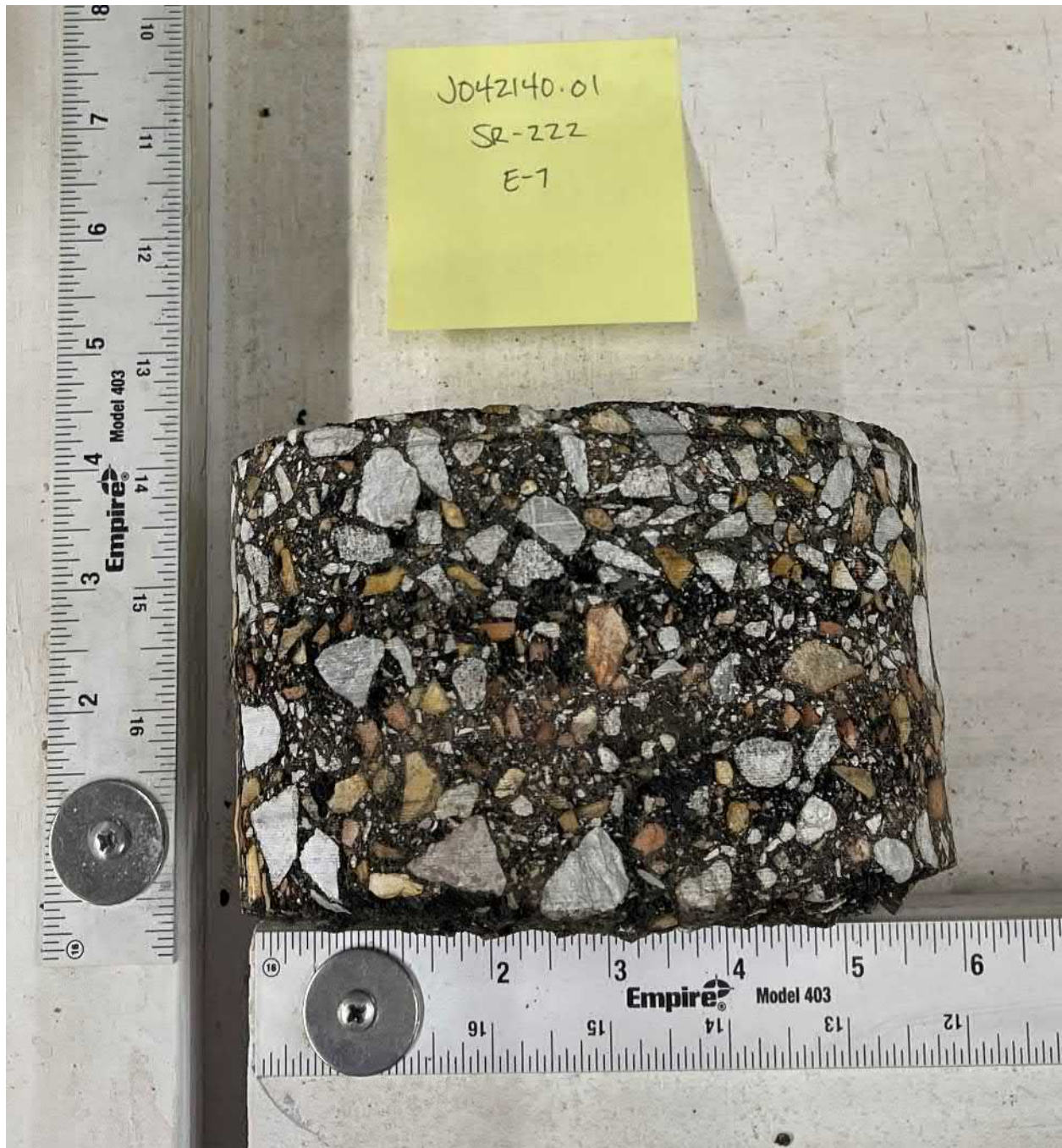




Appendix E
PAVEMENT CORE PHOTOGRAPHS



SR-222 From Near SR-468 to Near Campground Road	
Boring E-1	
J042140.01	Photograph 1
Description: 4½ inches of asphalt. Photograph taken on February 22, 2023.	



SR-222 From Near SR-468 to Near Campground Road	
Boring E-7	
J042140.01	Photograph 2
Description: 4¼ inches of asphalt. Photograph taken on February 22, 2023.	



SR-222 From Near SR-468 to Near Campground Road	
Boring W-5	
J042140.01	Photograph 3
Description: 4¾ inches of asphalt. Photograph taken on February 22, 2023.	



SR-222 From Near SR-468 to Near Campground Road	
Boring W-10	
J042140.01	Photograph 4
Description: 5 inches of asphalt. Photograph taken on February 22, 2023.	



SR-222 From Near SR-468 to Near Campground Road	
Boring W-21	
J042140.01	Photograph 5
Description: 17 inches of asphalt. Photograph taken on February 22, 2023.	